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Smart (Solid-State) Transformers Concepts/Challenges/Applications

J. W. Kolar et al.
Swiss Federal Institute of Technology (ETH) Zurich
Power Electronic Systems Laboratory
www.pes.ee.ethz.ch

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Smart (Solid-State) Transformers Concepts/Challenges/Applications

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Outline

- ► Transformer Basics
- ► Solid-State Transformer (SST) Concept
- ► Key SST Realization Challenges
  - #1 Power Semiconductors
  - #2 Topologies
  - #3 Medium Frequency Transformer
  - #4 Protection
  - #5 Reliability
- ► Industry Demonstrator Systems
- ► Potential Future Applications
- ► Conclusions

Acknowledgement: Dr. G. Ortiz

Transformer Basics

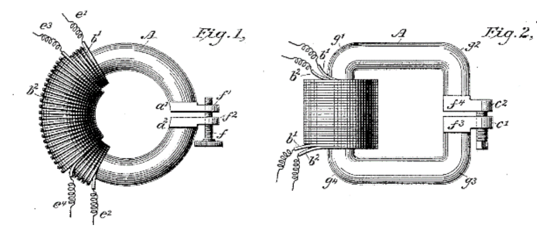
History
Scaling Laws
Efficiency / Power Density Trade-off

▶ Classical Transformer (XFMR) – History (1)

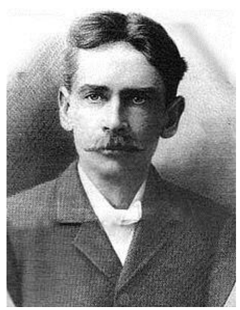
* 1830 - Henry/Faraday → Property of Induction
* 1878 - Ganz Company (Hungary) → Toroidal Transformer (AC Incandescent Syst.)
* 1880 - Ferranti → Early Transformer
* 1882 - Gaulard & Gibbs → Linear Shape XFMR (1884, 2kV, 40km)
* 1884 - Blathy/Zipernowski/Deri → Toroidal XFMR (inverse type)

Europe

USA



Patented Sept. 21, 1886. No. 349,611. W. STANLEY, Jr. INDUCTION COIL.



* 1885 - Stanley & (Westinghouse) → Easy Manufact. XFMR (1st Full AC Distr. Syst.)

► Classical Transformer – History (2)

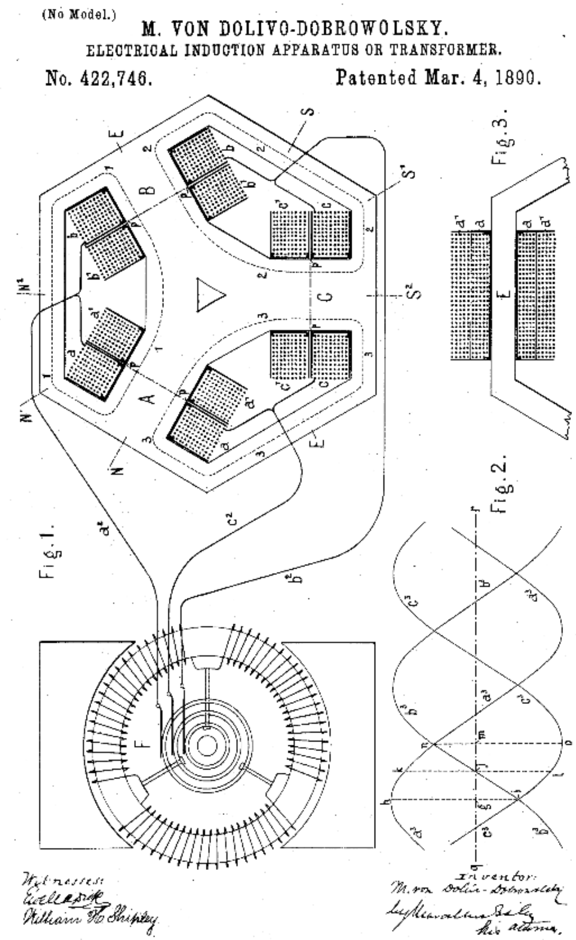
UNITED STATES PATENT OFFICE.

MICHAEL VON DOLIVO-DOBROWOLSKY, OF BERLIN, GERMANY, ASSIGNOR TO THE ALLGEMEINE ELEKTRICITÄTS-GESELLSCHAFT, OF SAME PLACE.

ELECTRICAL INDUCTION APPARATUS OR TRANSFORMER.

SPECIFICATION forming part of Letters Patent No. 422,746, dated March 4, 1890.

Application filed January 8, 1890. Serial No. 336,290. (No model.)



* 1889 - Dobrovolski → 3-Phase Transformer

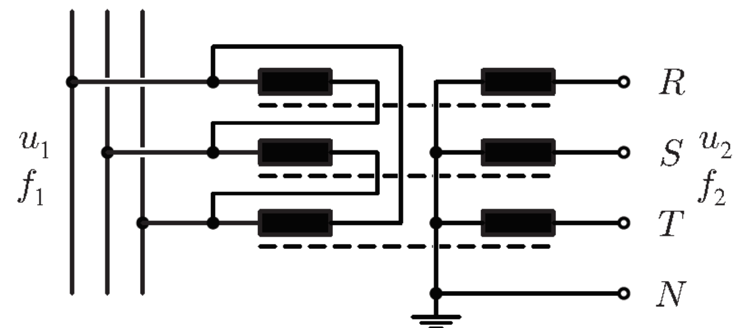
* 1891 - 1st Complete AC System (Gen.+XFMR+Transm.+El. Motor+Lamps, 40Hz, 25kV, 175km)

► Classical Transformer – Basics (1)

- Magnetic Core Material — * Silicon Steel / Nanocrystalline / Amorphous / Ferrite
- Winding Material — * Copper or Aluminium
- Insulation/Cooling — * Mineral Oil or Dry-Type

- Operating Frequency — * 50/60Hz (El. Grid, Traction) or $16^2/_3$ Hz (Traction)
- Operating Voltage — * 10kV or 20 kV (6…35kV)
  * 15kV or 25kV (Traction)
  * 400V

- Voltage Transf. Ratio — * Fixed
- Current Transf. Ratio — * Fixed
- Active Power Transf. — * Fixed ($P_1 \approx P_2$)
- React. Power Transf. — * Fixed ($Q_1 \approx Q_2$)
- Frequency Ratio — * Fixed ($f_1 = f_2$)

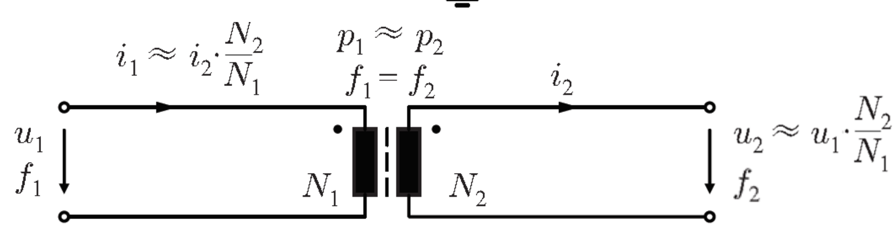


- Magnetic Core Cross Section

$$A_{Core} = \frac{1}{\sqrt{2}\pi}\frac{U_1}{\hat{B}_{max}\, f}\frac{1}{N_1}$$

- Winding Window

$$A_{Wdg} = \frac{2I_1}{k_W J_{rms}} N_1$$



▶ Classical Transformer – Basics (2)

Source: www.faceofmalawi.com

■ Advantages

- Relatively Inexpensive
- Highly Robust / Reliable
- Highly Efficient
- Short Circuit Current Limitation

▶ Classical Transformer – Basics (3)

Advantages

- Relatively Inexpensive
- Highly Robust / Reliable
- Highly Efficient (98.5%...99.5% Dep. on Power Rating)
- Short Circuit Current Limitation

Weaknesses

- Voltage Drop Under Load
- Losses at No Load
- Not Directly Controllable
- Dependency of Weight / Volume on Frequency
- Sensitivity to DC Offset Load Imbalances
- Sensitivity to Harmonics

- Construction Volume

$$A_{Core}A_{Wdg} = \frac{\sqrt{2}}{\pi}\frac{P_t}{k_W J_{rms} \hat{B}_{max} f}$$

↑ ↑ ↑

P_t .... Rated Power
k_W .... Window Utilization Factor
B_{max}.. Flux Density Amplitude
J_{rms}... Winding Current Density
f ..... Frequency

- Low Frequency → Large Weight / Volume

Vacuum Cast Coil Dry-Type Distribution Transformer

1 MVA – 12kV/400V @ 2600kg
0.2%/1% Losses @ No/Rated Load

▶ Classical Transformer – Basics (4)

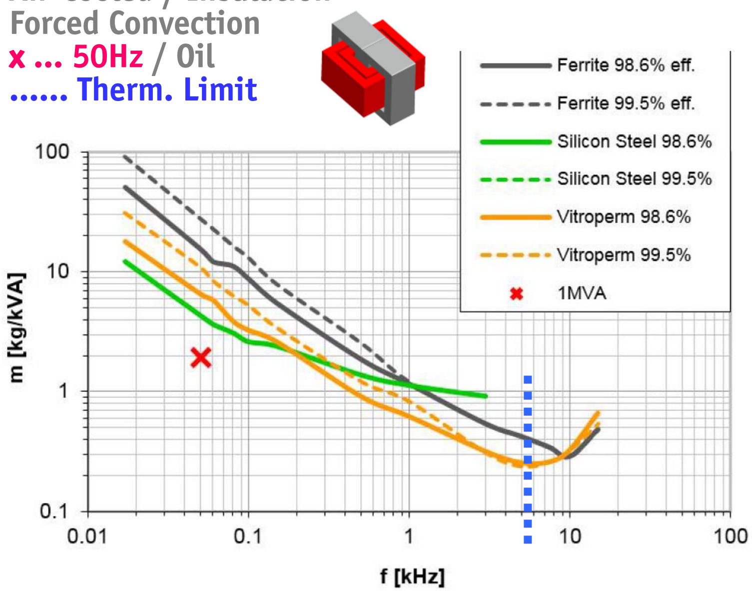
- **Construction Volume**

$$A_{Core}A_{Wdg} = \frac{\sqrt{2}}{\pi}\frac{P_t}{k_W J_{rms}\hat{B}_{max} f}$$

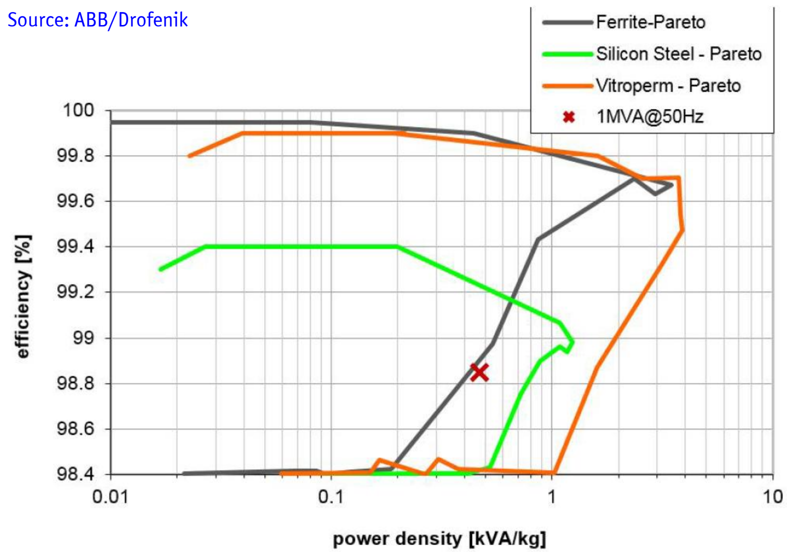
↑ ↑ ↑

P_t .... Rated Power
k_W .... Window Utilization Factor
B_{max}.. Flux Density Amplitude
J_{rms}... Winding Current Density
f ..... Frequency

180kVA
Weight-Optimized
Air-Cooled / Insulation
Forced Convection
x ... 50Hz / Oil
...... Therm. Limit



Source: ABB/Drofenik



- Higher Frequency → Lower Weight / Volume
- Higher Volume → Higher Efficiency

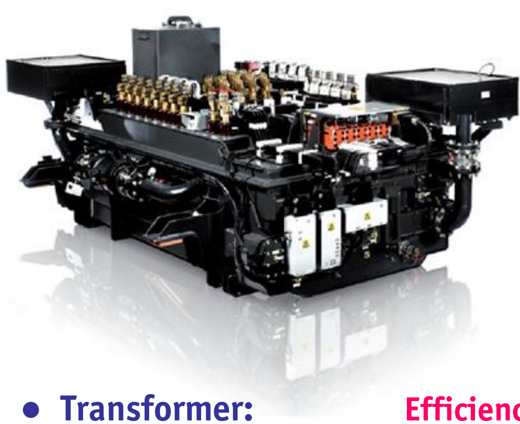
SST Motivation

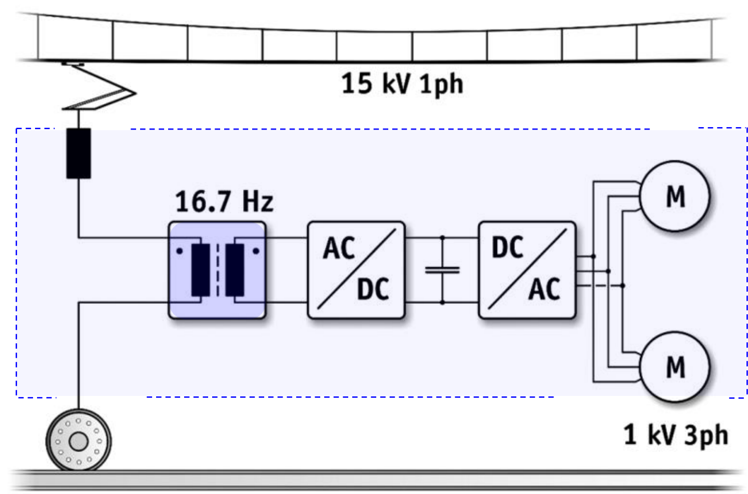
Next Generation Traction Vehicles

▶ Classical Locomotives

- Catenary Voltage 15kV or 25kV
- Frequency $16^2/_3$Hz or 50Hz
- Power Level 1...10MW typ.

Source: www.abb.com





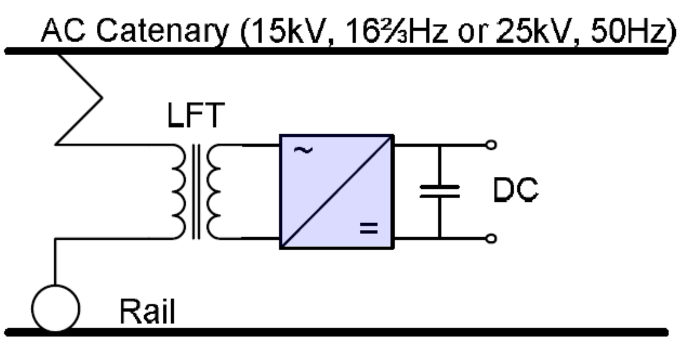
- Transformer:

Efficiency	90...95% (due to Restr. Vol., 99% typ. for Distr. Transf.)
Current Density	6 A/mm² (2A/mm² typ. Distribution Transformer)
Power Density	2...4 kg/kVA

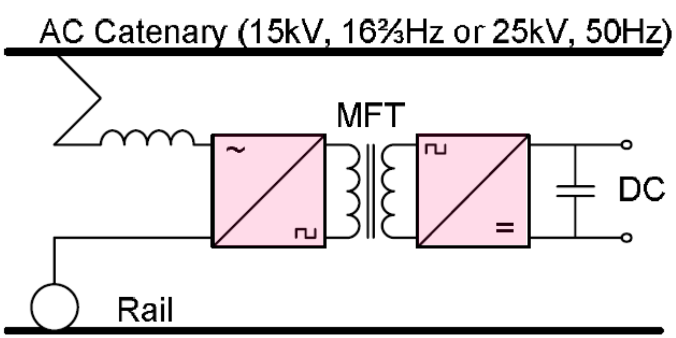
▶ Next Generation Locomotives

- Trends
  * Distributed Propulsion System → Volume Reduction (Decreases Efficiency)
  * Energy Efficient Rail Vehicles → Loss Reduction (Requires Higher Volume)
  * Red. of Mech. Stress on Track → Mass Reduction

Source: ABB



Conventional AC-DC conversion with a line frequency transformer (LFT).

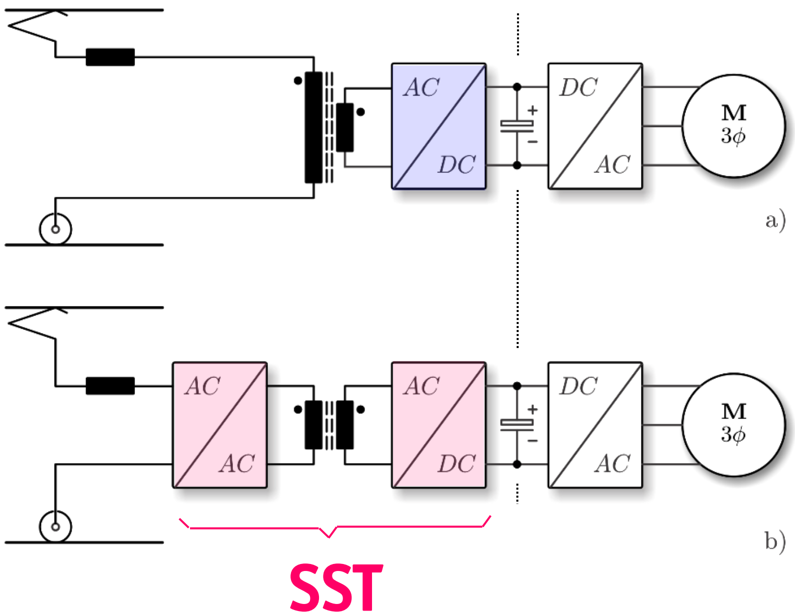


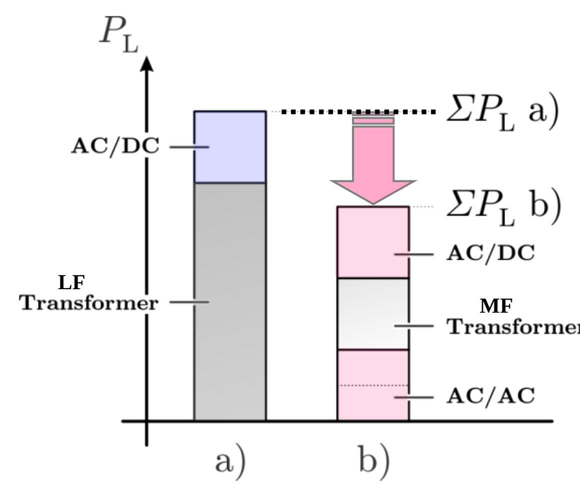
AC-DC conversion with medium frequency transformer (MFT).

- Replace LF Transformer by *Medium Frequency* Power Electronics Transformer → **SST**
- *Medium Frequency* Provides Degree of Freedom → Allows Loss Reduction *AND* Volume Reduction

▶ Next Generation Locomotives

- Loss Distribution of Conventional & Next Generation Locomotives





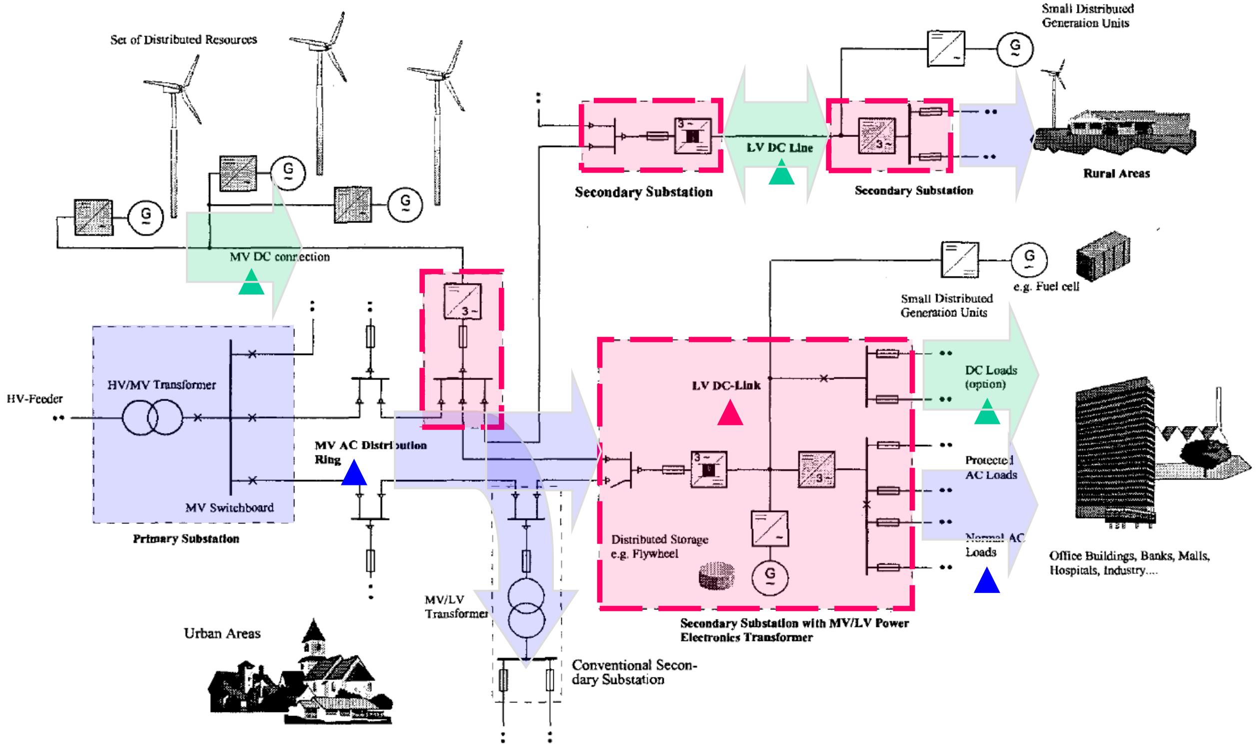
- Medium Frequ. Provides Degree of Freedom → Allows Loss Reduction *AND* Volume Reduction

Future Smart EE Distribution

Source: TU Munich

▶ Advanced (High Power Quality) Grid Concept

- Heinemann / ABB (2001)



- MV AC Distribution with DC Subsystems (LV and MV) and Large Number of Distributed Resources
- MF AC/AC Conv. with DC Link Coupled to Energy Storage provide High Power Qual. for Spec. Customers

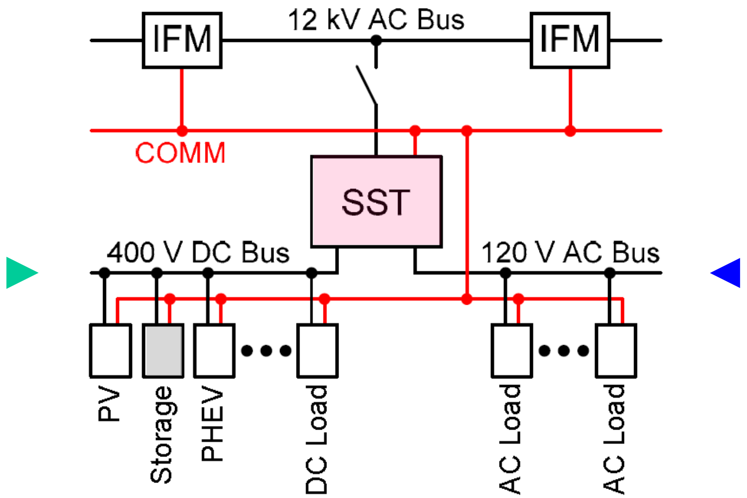
► Future Ren. Electric Energy Delivery & Management (FREEDM) Syst.

- Huang et al. (2008)

● SST as Enabling Technology for the "Energy Internet"

- Full Control of the Power Flow
- Integr. of DER (Distr. Energy Res.)
- Integr. of DES (Distr. E-Storage) + Intellig. Loads
- Protects Power Syst. From Load Disturbances
- Protects Load from Power Syst. Disturbances
- Enables Distrib. Intellig. through COMM
- Ensure Stability & Opt. Operation
- etc.
- etc.

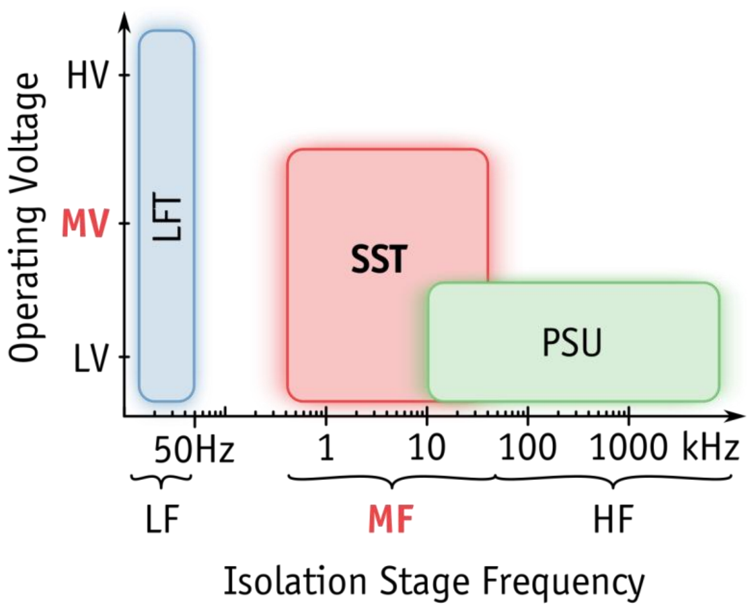
IFM = Intellig. Fault Management

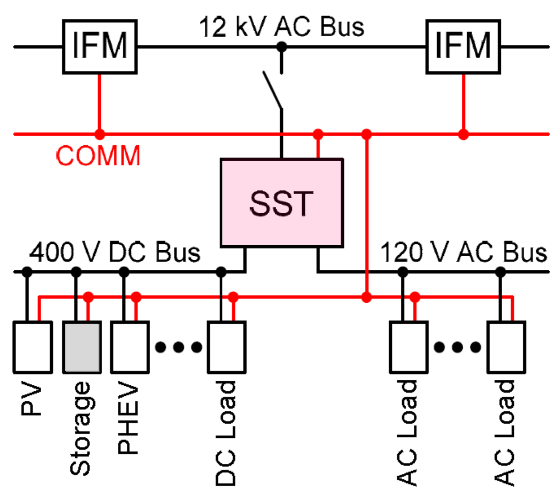


● Bidirectional Flow of Power & Information / High Bandw. Comm. → Distrib. / Local Autonomous Cntrl

▶ Terminology (1)

McMurray	Electronic Transformer (1968)
Brooks	Solid-State Transformer (SST, 1980)
EPRI	Intelligent Universal Transformer (IUT™)
ABB	Power Electronics Transformer (PET)
Borojevic	Energy Control Center (ECC)
Wang	Energy Router
etc.	





▶ Terminology (1)

United States Patent [19] [11] **4,347,474**

Brooks et al. [45] **Aug. 31, 1982**

[54] SOLID STATE REGULATED POWER TRANSFORMER WITH WAVEFORM CONDITIONING CAPABILITY ← "... Solid State Regulated Power Transformer ..."

[75] Inventors: **James L. Brooks**, Oxnard; **Roger I. Staab**, Camarillo, both of Calif.; **James C. Bowers**; **Harry A. Nienhaus**, both of Tampa, Fla.

[73] Assignee: **The United States of America as represented by the Secretary of the Navy**, Washington, D.C.

[21] Appl. No.: **188,419**

[22] Filed: **Sep. 18, 1980**

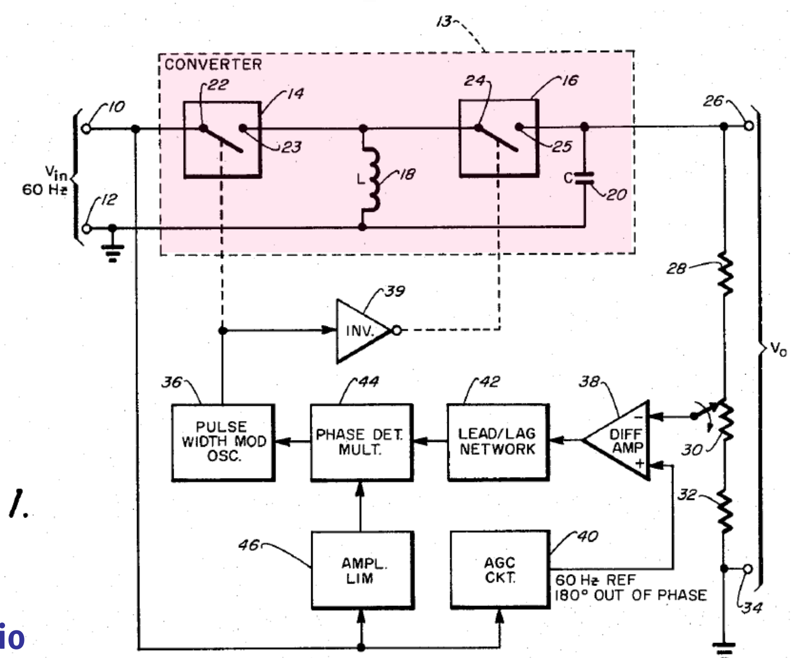
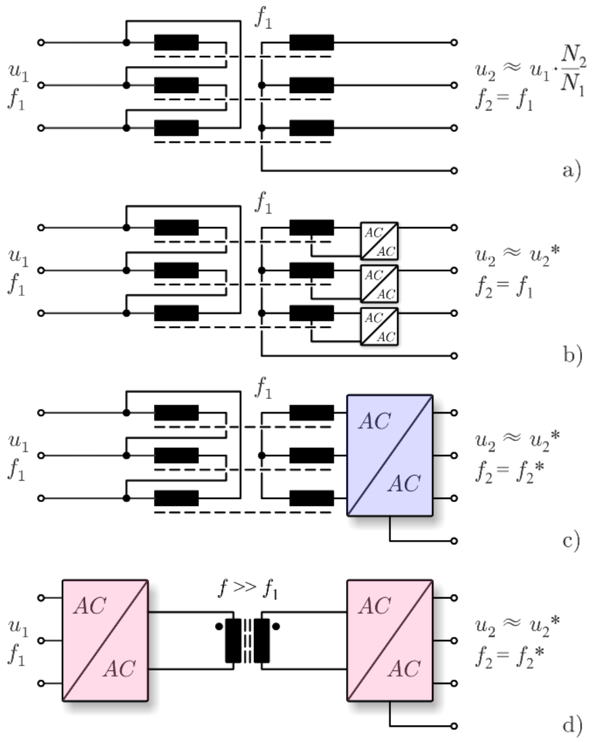


Fig. 1.

- No Isolation (!)
- "Transformer" with Dyn. Adjustable Turns Ratio

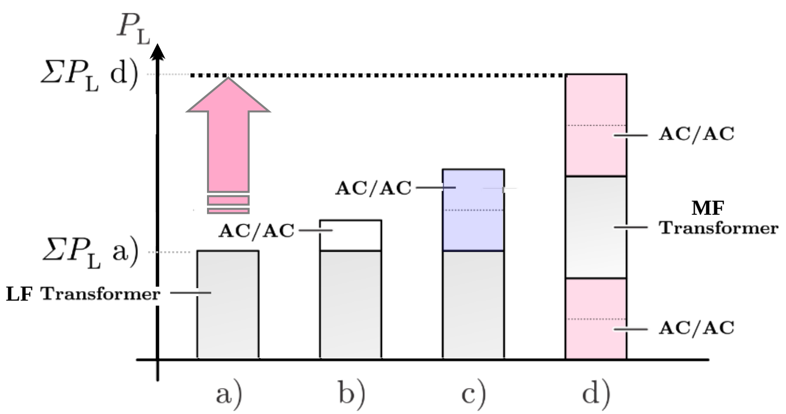
▶ Passive Transformer → SST

- Efficiency Challenge



LF Isolation
Purely Passive (a)
Series Voltage Comp. (b)
Series AC Chopper (c)

MF Isolation
Active Input & Output Stage (d)



- Medium Freq. → Higher Transf. Efficiency Partly Compensates Converter Stage Losses
- Medium Freq. → Low Volume, High Control Dynamics

SST Concept Implementation

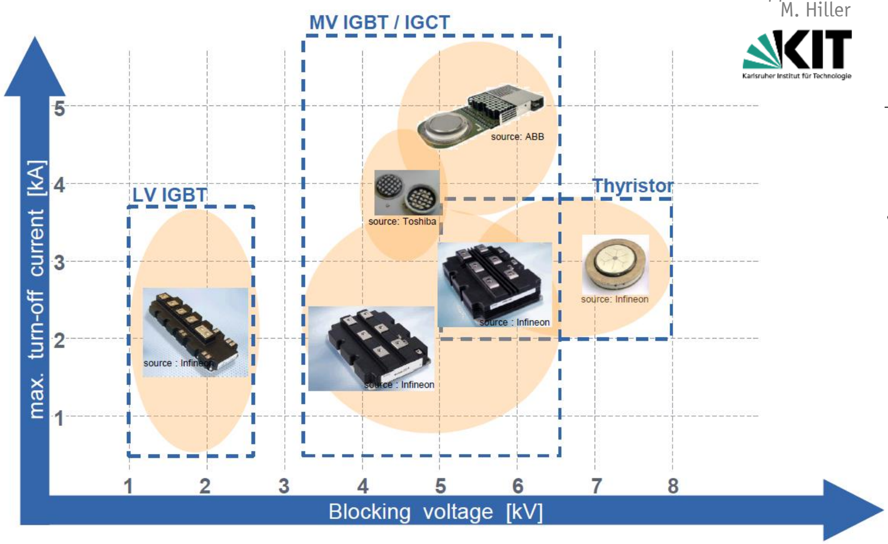
Challenge #1/5

Availability / Selection of Power Semiconductors

▶ Available Si Power Semiconductors

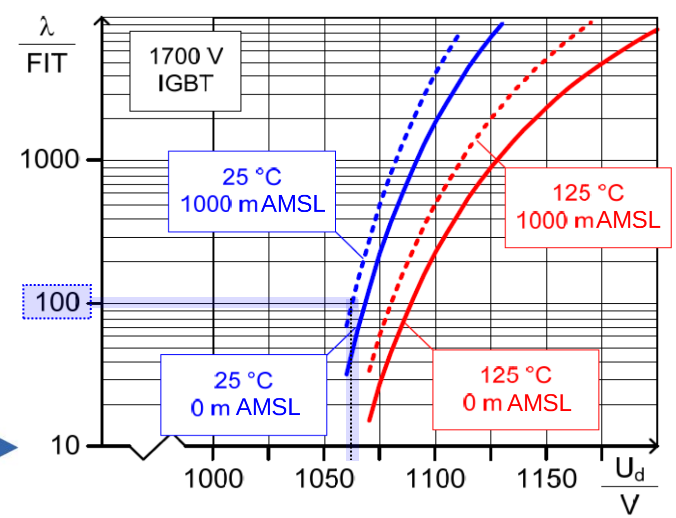
- 1200V/1700V Si-IGBTs Most Frequently Used in Industry Applications

Source: M. Doppelbauer M. Hiller



- Derating Requirement due to Cosmic Radiation 1700V Si-IGBTs → ≈1000V max. DC Voltage

Source: H.-G. Eckel Univ. Rostock

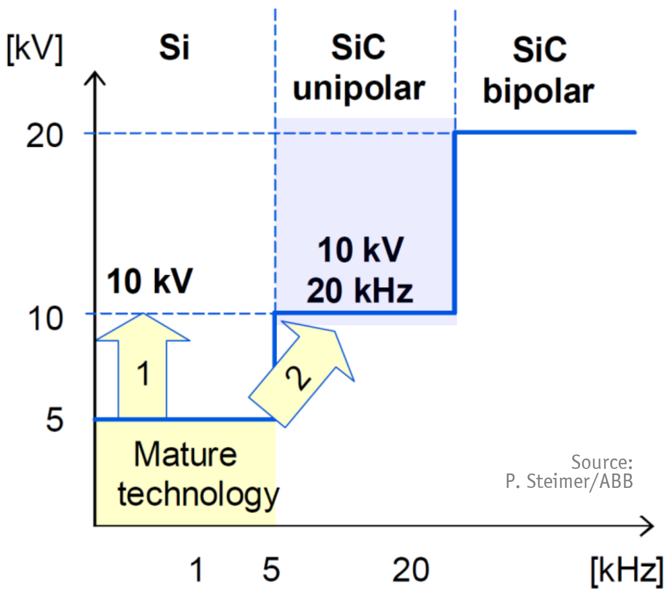


- Interfacing to Medium Voltage → Multi-Level Converter Topologies

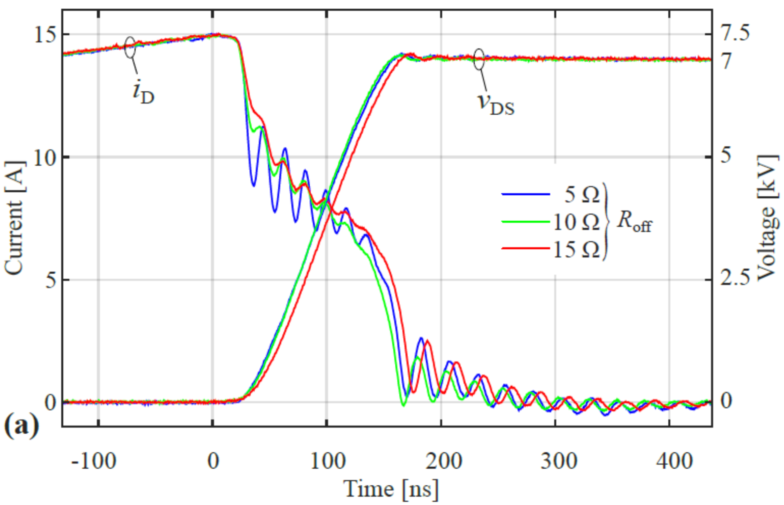
▶ SiC Power Semiconductors

- Samples

* 10kV & 15kV / 10A MOSFETs
* 10kV & 15kV / 8A JBS Diodes
* 15kV / 20A IGBTs



- Soft-Switching (ZVS) Performance
  10kV MOSFET @ 15A
  (250uJ)



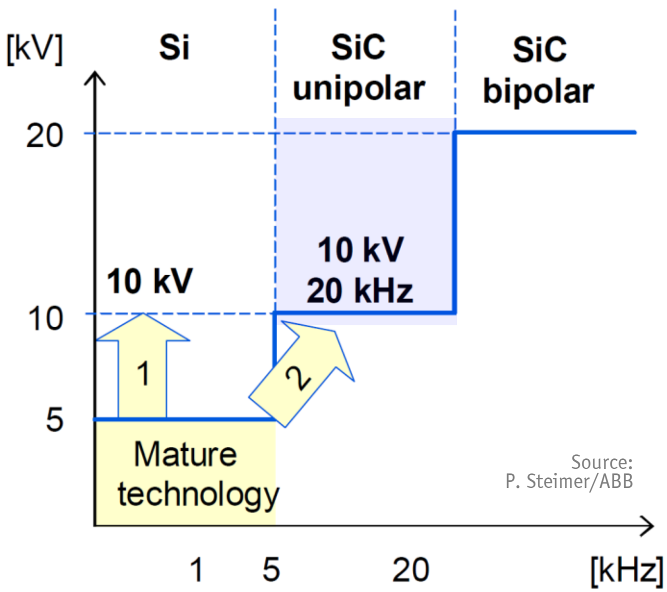
- Interfacing to Medium Voltage → Two-Level *OR* Multi-Level Converter Topologies

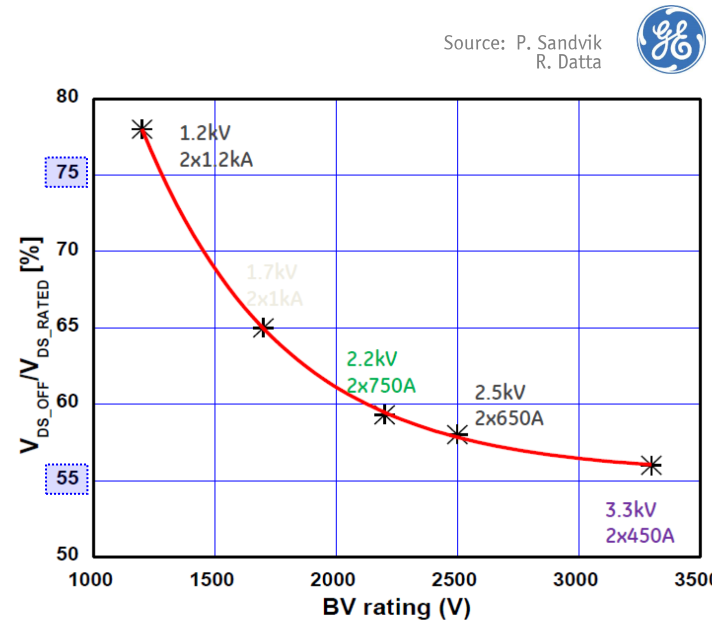
▶ SiC Power Semiconductors

- **Samples** Wolfspeed

* 10kV & 15kV / 10A MOSFETs
* 10kV & 15kV / 8A JBS Diodes
* 15kV / 20A IGBTs

- **Derating Requirement due to Cosmic Radiation for 100 FIT @ 25°C & 0 m AMSL A_{act}=7.2cm²**

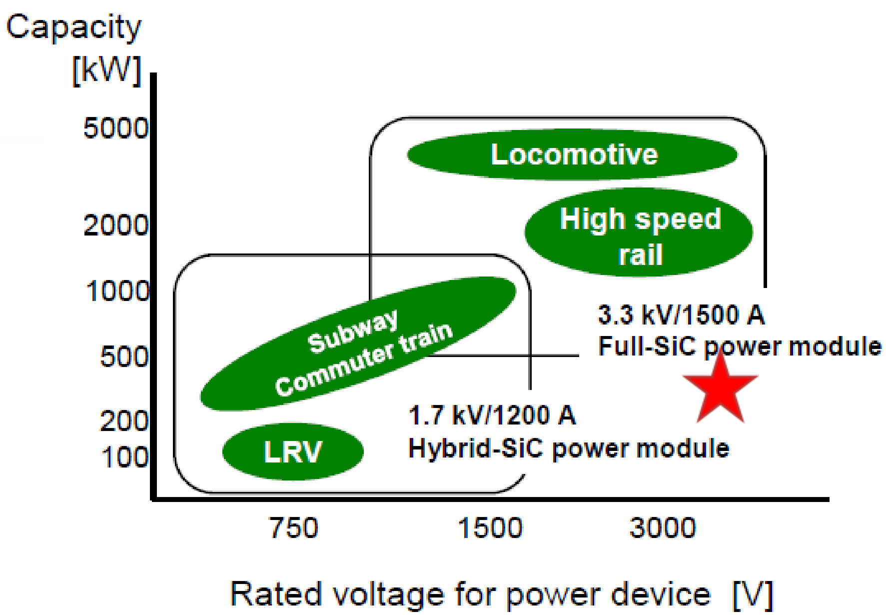


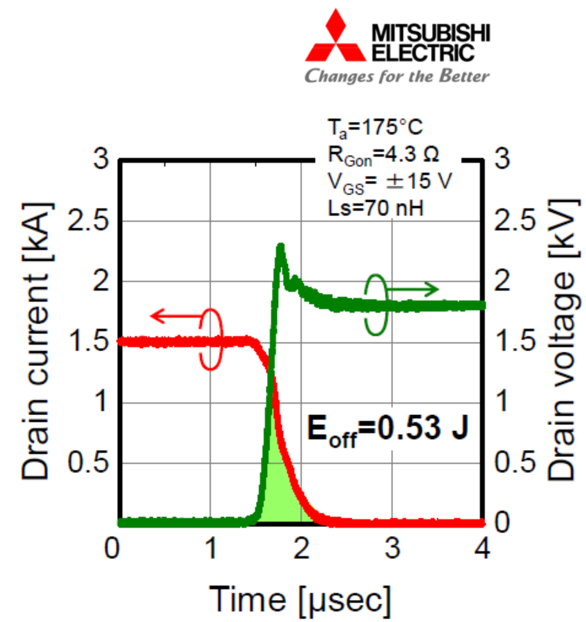


■ Interfacing to Medium Voltage → Two-Level *OR* Multi-Level Converter Topologies

▶ Commercially Available SiC Power Semiconductors

- High Current 3.3kV / 1.7kV / 1.2 kV Power Modules
- Mitsubishi (CREE, ROHM, GE, etc.)

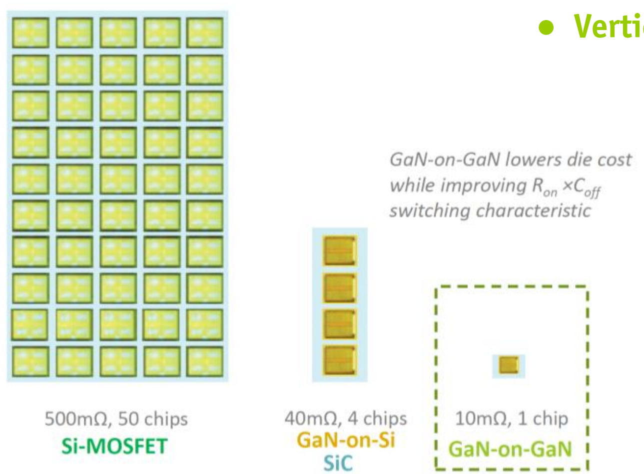




▶ Vertical (!) FETs on Bulk GaN Substrates

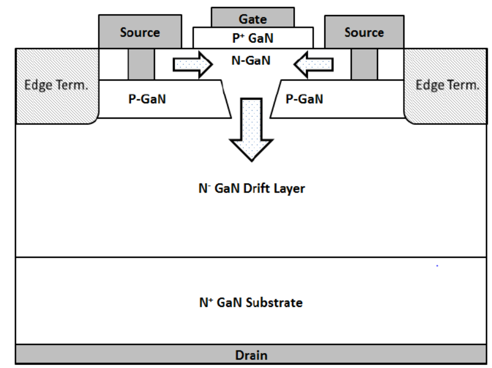
■ GaN-on-GaN Means Less Chip Area

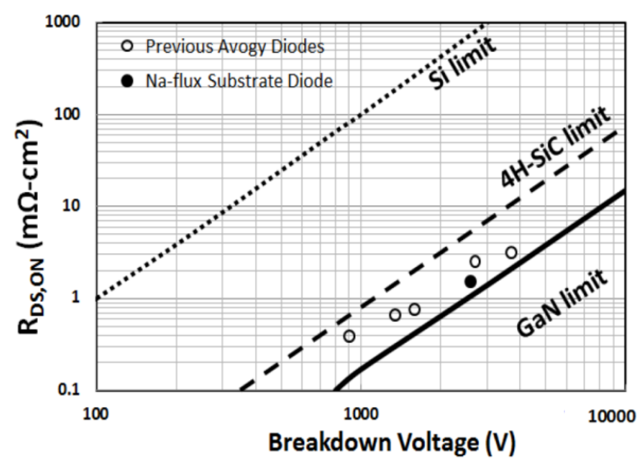
For a given on-resistance (R_{on}) of 10mΩ:



Breakdown Voltage (V)	Doping(cm-3)	Drift Length (μm)
600	4.8×10^{16}	3.7
1200	2.4×10^{16}	7.3
1800	1.6×10^{16}	10.9
2400	1.2×10^{16}	14.6
3200	0.9×10^{16}	19.4
4800	0.6×10^{16}	29.1
5600	0.5×10^{16}	34.0

● Vertical FET Structure





Challenge #2/5

*Creation of MV → LV
SST Topologies*

▶ Interfacing to Medium Voltage

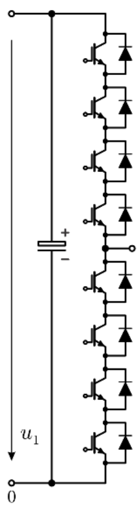
- Partitioning of Blocking Voltage
- Series Connection or Multi-Cell and Multi-Level Approaches
- High Number *N* Cells → Quadratically Reduces Curr. Harmonics

Marquardt

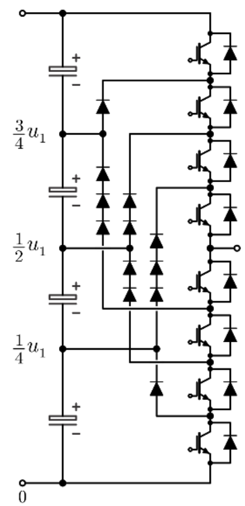
Alesina/ Venturini (1981)

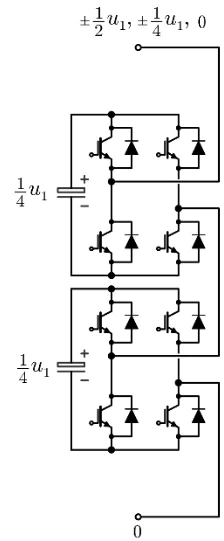
Akagi (1981)

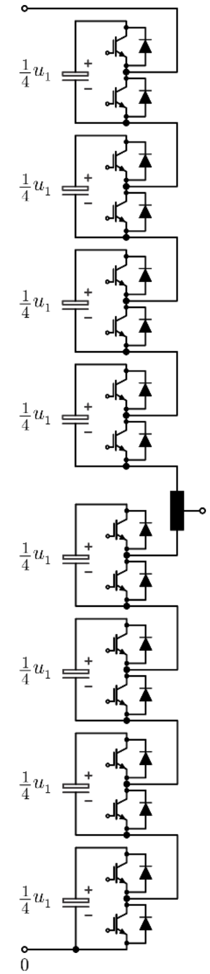
McMurray (1969)



* Two-Level Topology



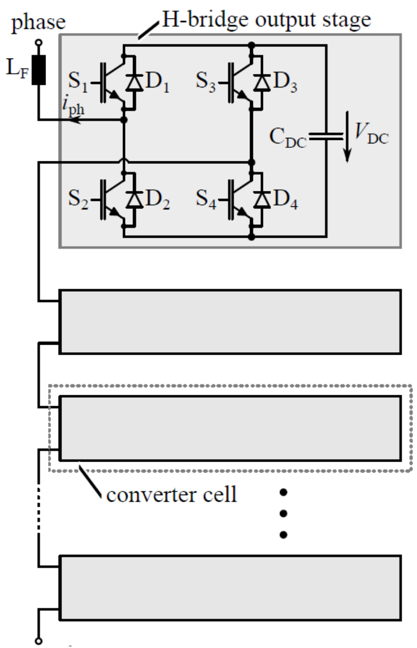


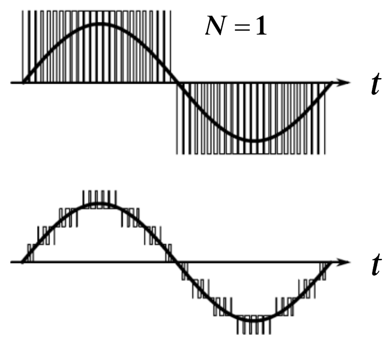


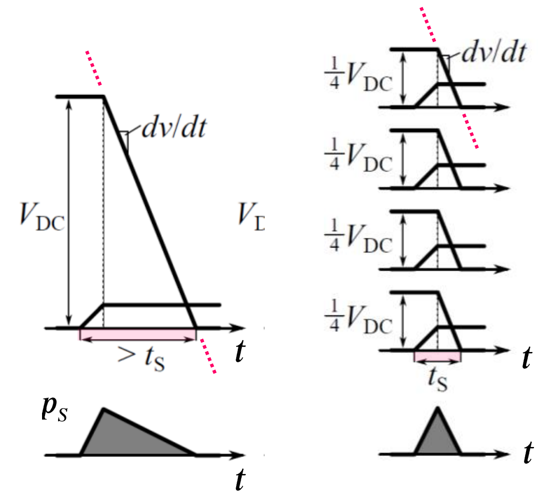
* Multi-Level/ Multi-Cell Topologies

► Scaling of Series Interleaving of Converter Cells

- **Interleaved Series Connection Dramatically Reduces Switching Losses (or Harmonics)**







– **Scaling of Switching Losses for Equal $\Delta i/I$ and dv/dt**

$$P_{S,N} \approx P_{S,N=1} \cdot \left(\frac{1}{2N^2} \cdots \frac{1}{N^3}\right)$$

- **Converter Cells Could Operate at VERY Low Switching Frequency**
- **Minimization of Passives (Filter Components)**

United States Patent [11] 3,581,212

[54] **FAST RESPONSE STEPPED-WAVE SWITCHING POWER CONVERTER CIRCUIT**
18 Claims, 13 Drawing Figs.

[72]	Inventor	**William McMurray** **Schenectady, N.Y.**
[21]	Appl. No.	**846,354**
[22]	Filed	**July 31, 1969**
[45]	Patented	**May 25, 1971**
[73]	Assignee	**General Electric Company**

← 1969 !

Inventor:
William McMurray,
by Donald R. Campbell
His Attorney.

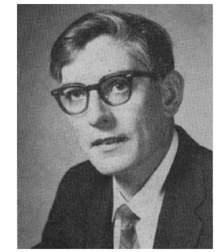
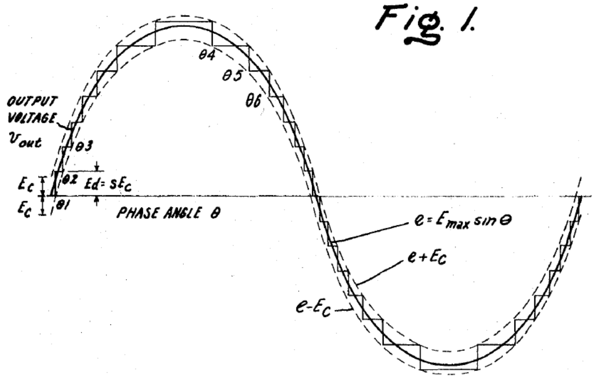
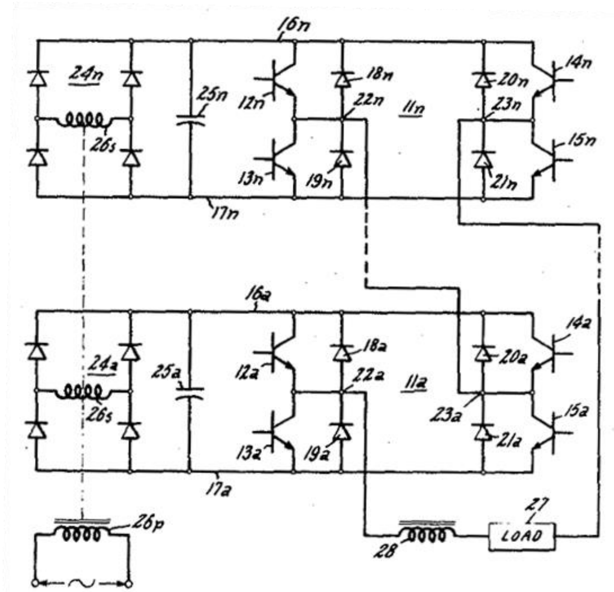


Fig. 1.





- Cascaded H-Bridge Multi-Cell Converter

United States Patent Office

3,517,300
Patented June 23, 1970

1

3,517,300

POWER CONVERTER CIRCUITS HAVING A HIGH FREQUENCY LINK

William McMurray, Schenectady, N.Y., assignor to General Electric Company, a corporation of New York

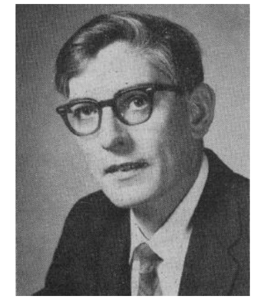
Filed Apr. 16, 1968, Ser. No. 721,817
Int. Cl. H02m 5/16, 5/30
U.S. Cl. 321—60 14 Claims

ABSTRACT OF THE DISCLOSURE

Several single phase solid state power converter circuits have a high frequency transformer link whose windings are connected respectively to the load and to a D-C or low frequency A-C source through inverter configuration switching circuits employing inverse-parallel pairs of controlled turn-off switches (such as transistors or gate turn-off SCR's) as the switching devices. Filter means are connected across the input and output terminals. By synchronously rendering conductive one switching device in each of the primary and secondary side circuits, and alternately rendering conductive another device in each switching circuit, the input potential is converted to a high frequency wave, transformed, and reconstructed at the output terminals. Wide range output voltage control is obtained by phase shifting the turn-on of the switching devices on one side with respect to those on the other side by 0° to 180°, and is used to effect current limiting, current interruption, current regulation, and voltage regulation.

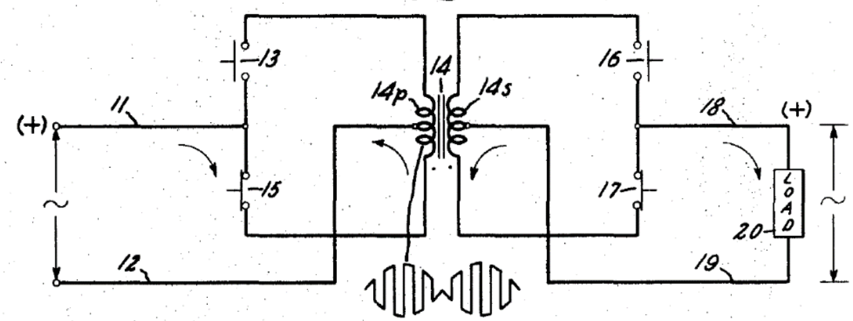
1968 !

Filed April 16, 1968



Inventor:
William McMurray,
by Donald R. Campbell
His Attorney.

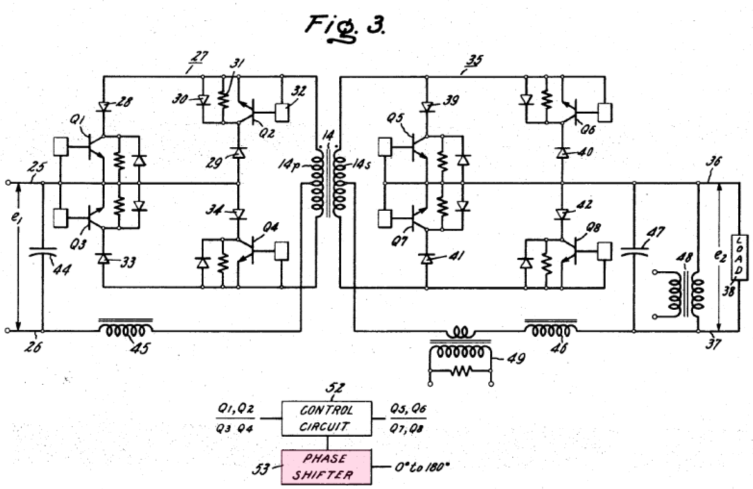
Fig. 1a

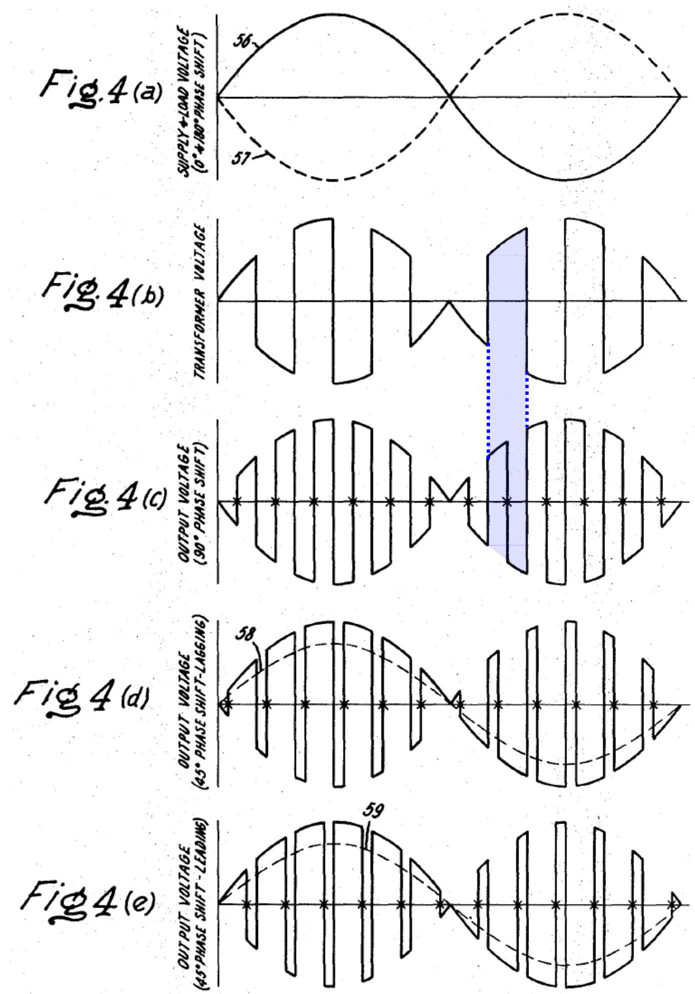


- Electronic Transformer ($f_1 = f_2$)
- AC or DC Voltage Regulation & Current Regulation/Limitation/Interruption

► Electronic Transformer

- Inverse-Paralleled Pairs of Turn-off Switches
- 50% Duty Cycle of Input and Output Stage





- $f_1 = f_2$ → Not Controllable (!)
- Voltage Adjustment by Phase Shift Control (!)

United States Patent [19] [11] **Patent Number: 5,027,264**

DeDoncker et al. [45] **Date of Patent: Jun. 25, 1991** ← **1991**

[54] **POWER CONVERSION APPARATUS FOR DC/DC CONVERSION USING DUAL ACTIVE BRIDGES** ← "… Dual Active Bridges …"

[75] Inventors: **Rik W. DeDoncker**, Niskayuna, N.Y.; **Mustansir H. Kheraluwala; Deepakraj M. Divan**, both of Madison, Wis.

[22] Filed: **Sep. 29, 1989**

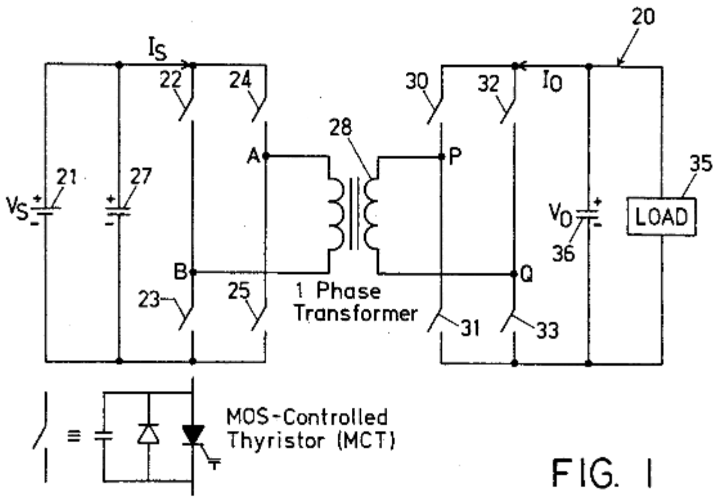


FIG. 1

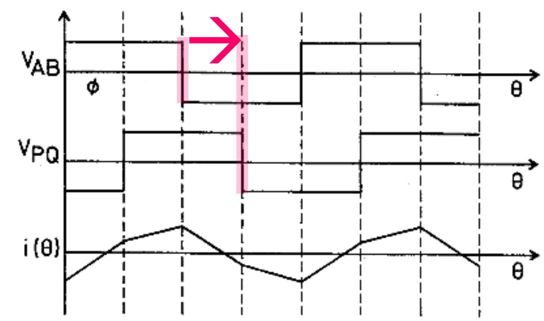


FIG. 2

- Soft Switching in a Certain Load Range
- Power Flow Control by Phase Shift between Primary & Secondary Voltage

IEEE TRANSACTIONS ON INDUSTRIAL ELECTRONICS AND CONTROL INSTRUMENTATION VOL. IECI-17, NO. 3, MAY 1970 ← 1970 !

A Method of Resonant Current Pulse Modulation for Power Converters

FRANCISC C. SCHWARZ, SENIOR MEMBER, IEEE

- **Load-Insensitive DCM Series Resonant Converter**

- Resonant Tank

- Transformer Voltage
- Transformer Current

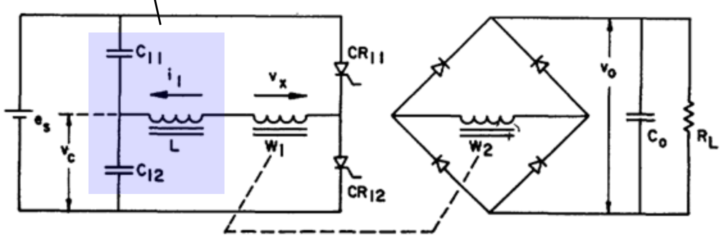
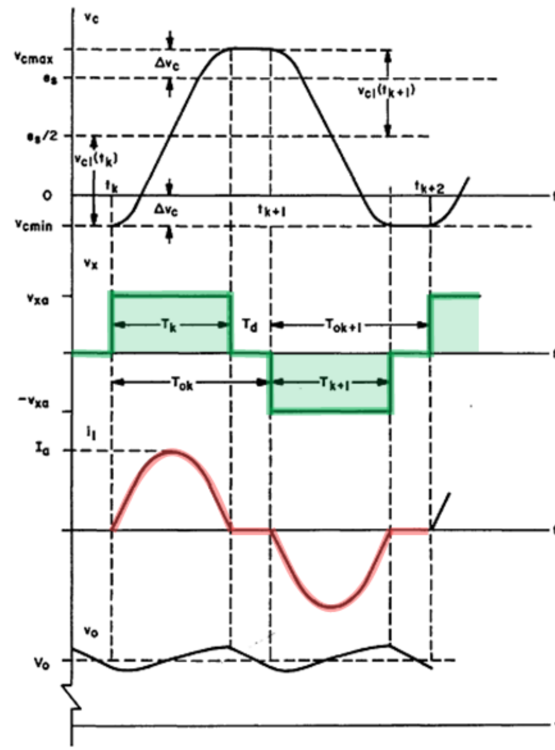
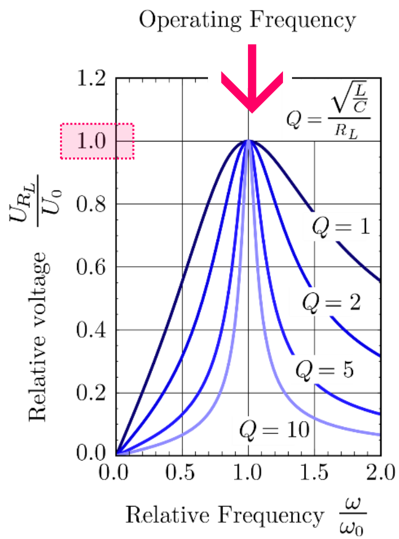


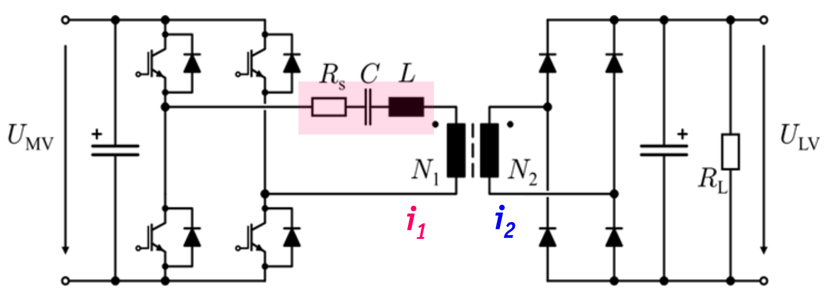
Fig. 4. Alternative simplified schematic of a controllable and load-insensitive series capacitor dc converter with transfer of inductive energy to the load.

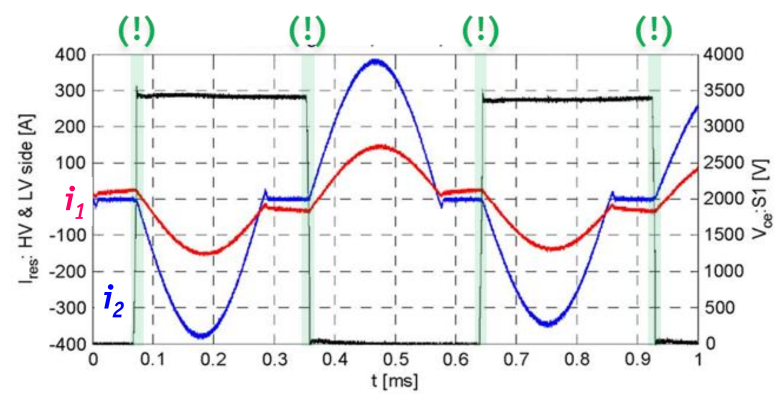


► Half-Cycle DCM Series Resonant Converter (HC-DCM-SRC)

- $f_S \approx$ Resonant Frequency → "Unity Gain"
- Fixed Voltage Transfer Ratio Independent of Transferred Power (!)
- Power Flow / Power Direction Self-Adjusting
- No Controllability / No Need for Control
- ZCS of All Devices



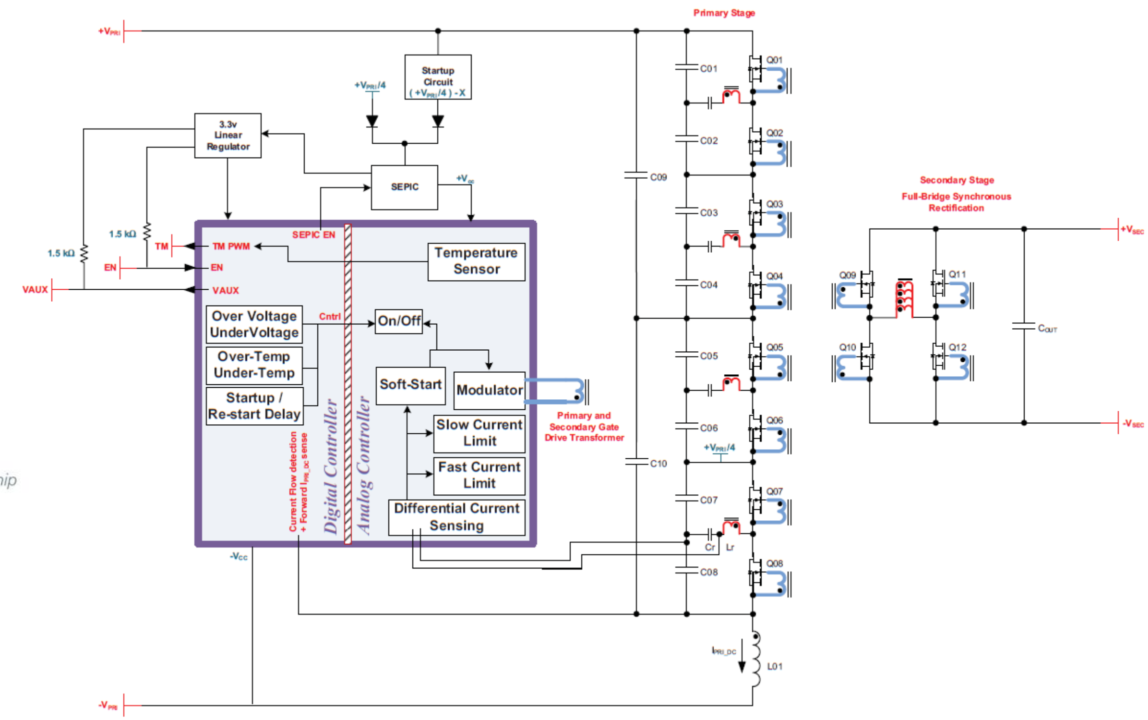




► Remark: Concept also Used for Low-Power (!)

- BCM Bus Converter Family
- Sine Amplitude Converter (SAC)
- Fixed Voltage Conversion Ratio DC/DC Converter

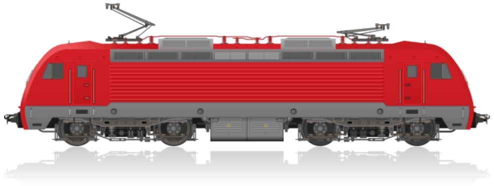
VICOR



- Very High Power Density
- Very High Efficiency

Combining the Basic Concepts I

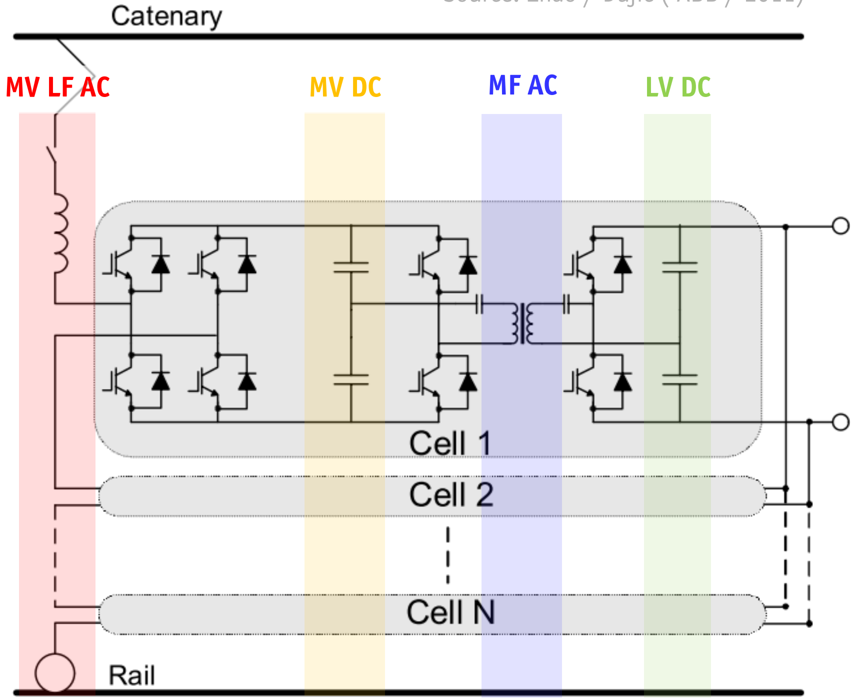
Single-Phase AC-DC Conversion / Traction Applications

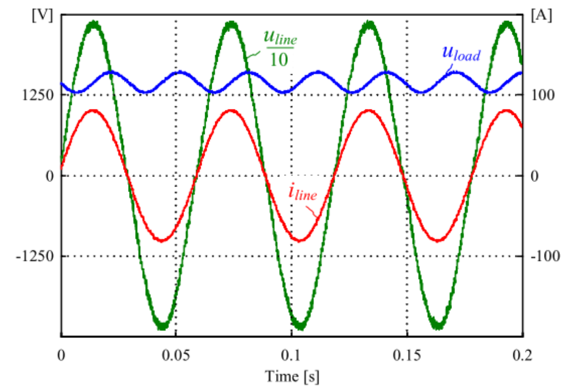


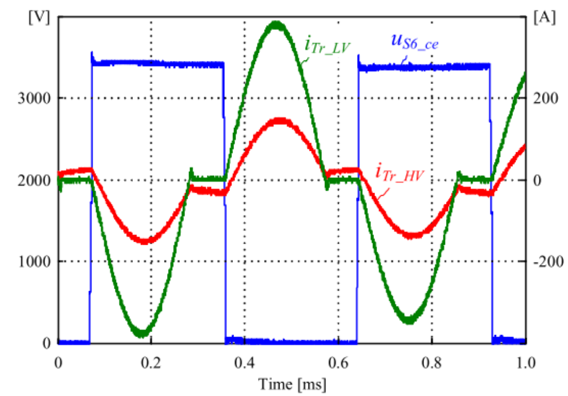
▶ Cascaded H-Bridges w. Isolated Back End

- Multi-Cell Concept (AC/DC Front End & Soft-Switching Resonant DC//DC Converter)
- Input Series / Output Parallel Connection – Self Symmetrizing (!)
- Highly Modular / Scalable
- Allows for Redundancy
- High Power Demonstrators: ABB BOMBARDIER ALSTOM etc.

Source: Zhao / Dujic (ABB / 2011)

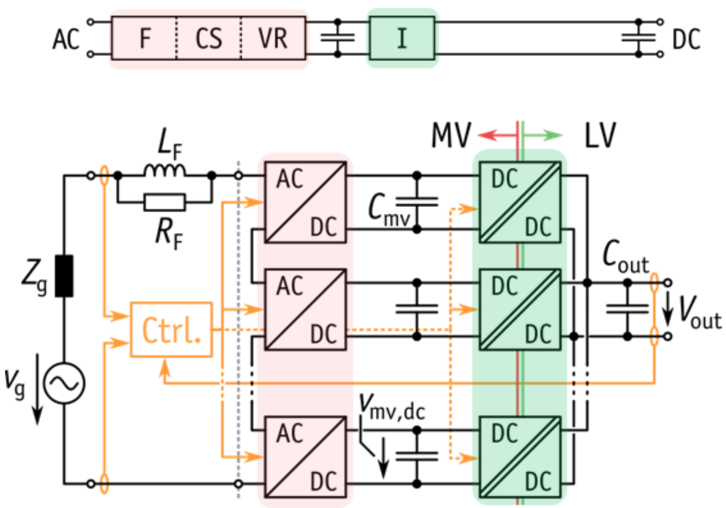






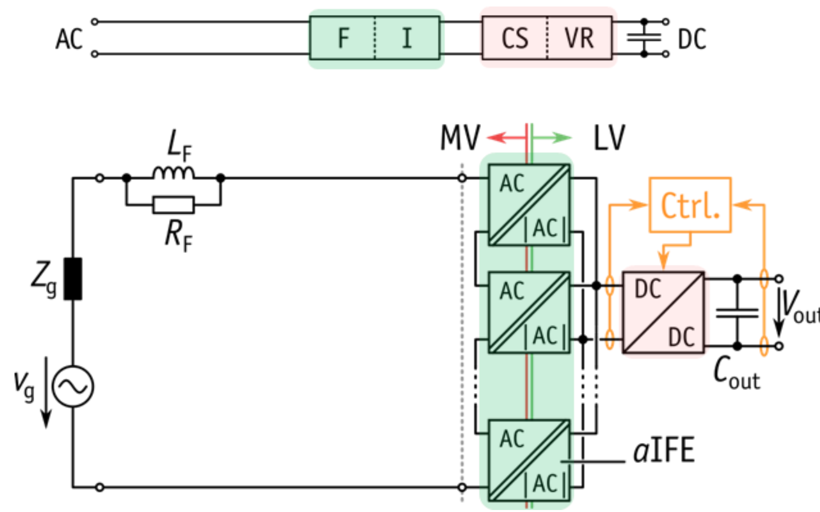
Reversal of the Sequence of Current Shaping & Isolation

Isolated DC/DC Back End



- Typical Multi-Cell SST Topology
- Two-Stage Multi-Cell Concept
- Direct Input Current Control
- Indirect Output Voltage Control
- High Complexity at MV Side

Isolated AC/|AC| Front End

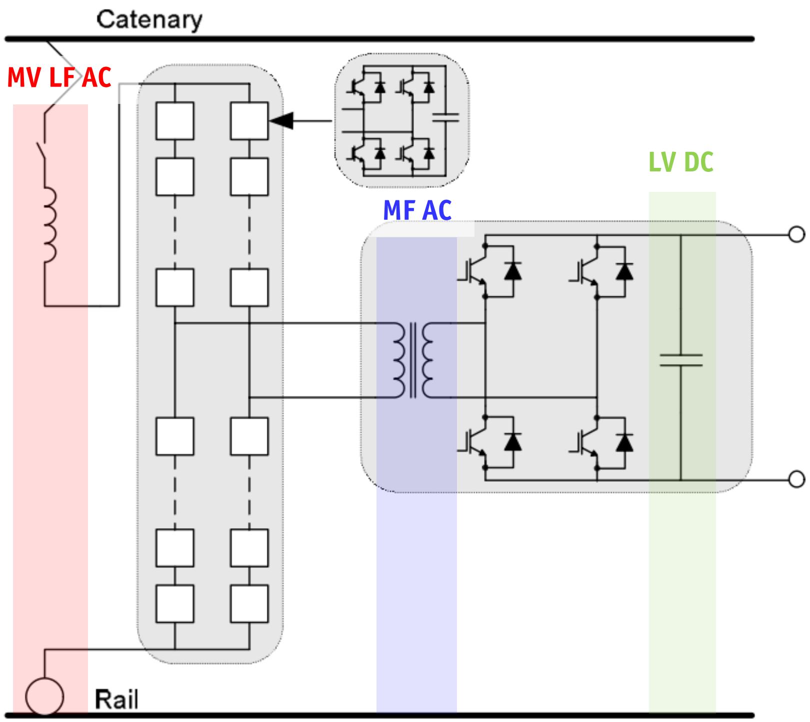


- Swiss SST (S3T)
- Two-Stage Multi-Cell Concept
- Indirect Input Current Control
- Direct Output Voltage Control
- Low Complexity on MV Side

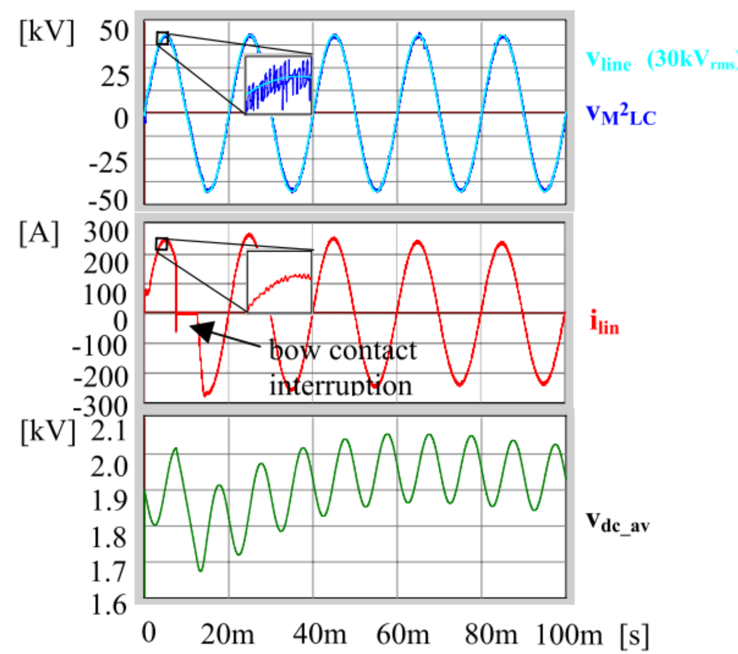
▶ Modular Multilevel Converter

- Single Transformer Isolation
- Highly Modular / Scalable
- Allows for Redundancy
- Challenging Balancing on Cell DC Voltages

SIEMENS
- Marquardt/Glinka (2003)

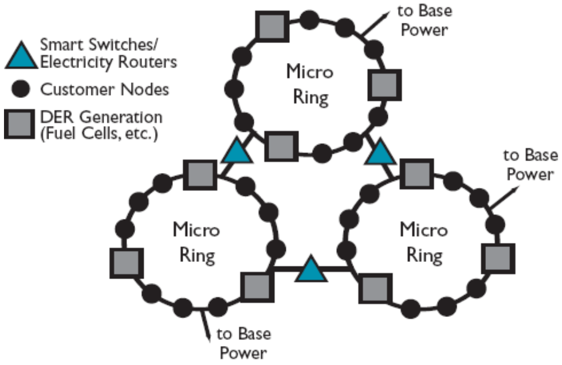


Source: Zhao / Dujic (ABB / 2011)



Combining the Basic Concepts II

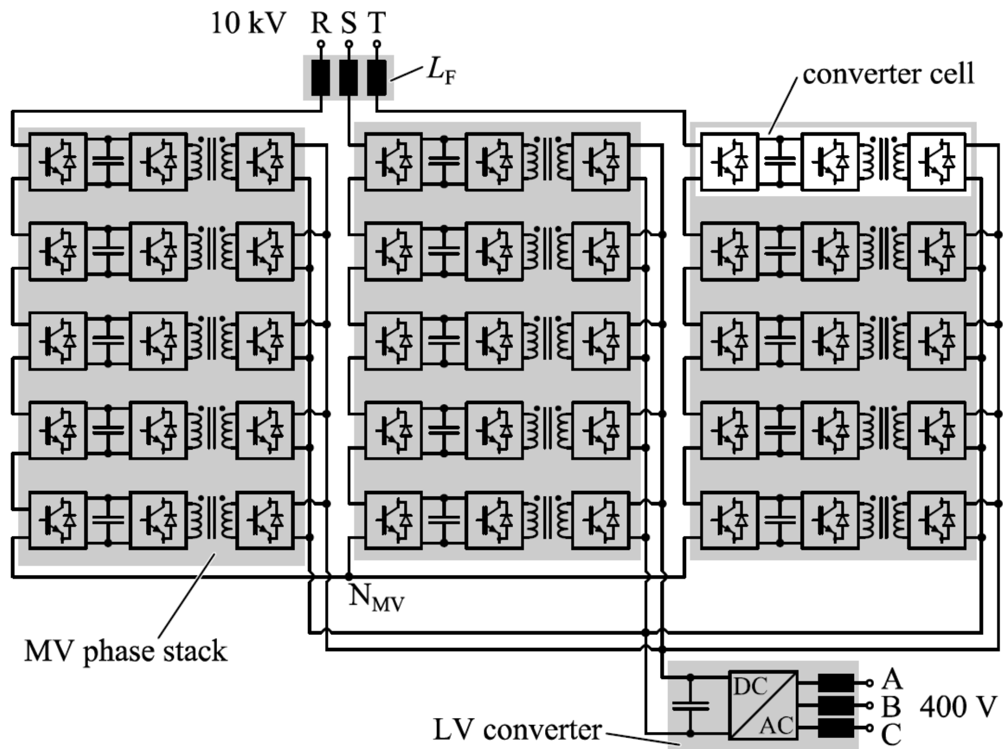
Three-Phase AC-AC Conversion / Smart Grid Applications



Source: EPRI ELECTRIC POWER RESEARCH INSTITUTE

▶ MEGALink @ ETH Zurich

S_N = 630kVA
U_{LV} = 400 V
U_{MV} = 10kV

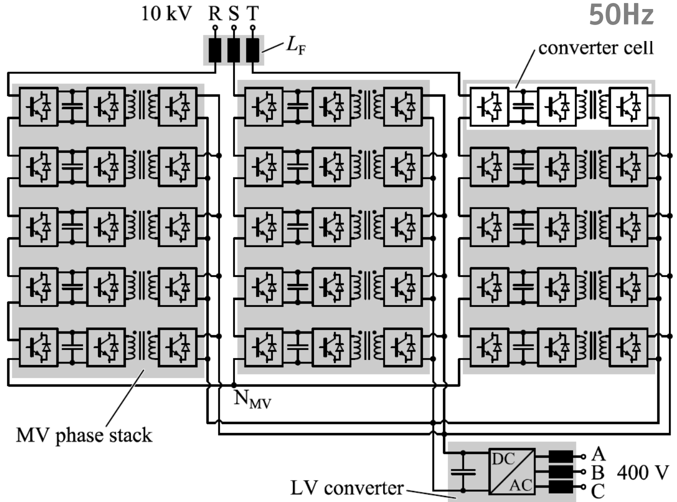


- 2-Level Inverter on LV Side
- HC-DCM-SRC DC//DC Conversion
- Cascaded H-Bridge MV Structure – ISOP Topology

▶ Optimum Number of Converter Cells

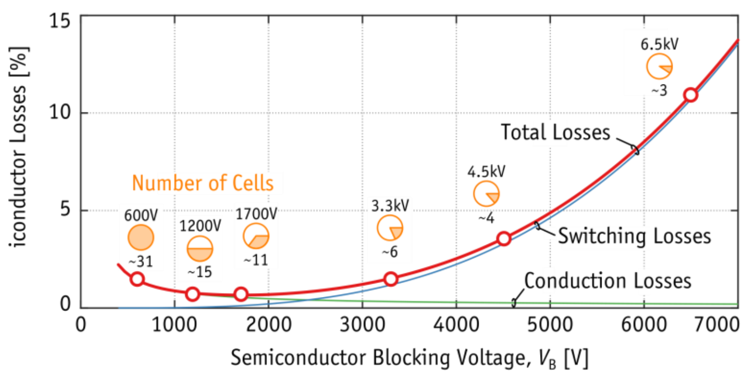
1 MVA
10kV → 400V
50Hz

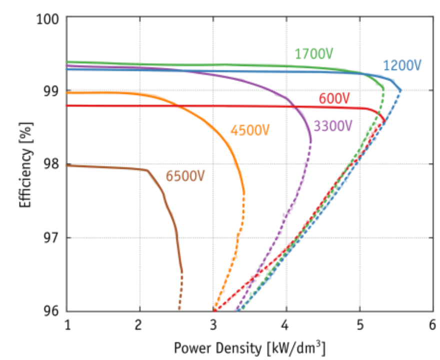
■ **Trade-Off** High Number of Levels →
High Conduction Losses/
Low Cell Sw. Frequ./Losses
(also because of Device Char.)



- Opt. Device Voltage Rating for Given MV Level
- ηρ-Pareto Opt. (Compliance to IEEE 519 @ Eff. Sw. Frequ., only Cascaded H-Bridges, i.e. DC/DC Converter Stages Not Considered)

L_F=10%
$\Delta \hat{i}_{pp}/\hat{I}_N$=1%

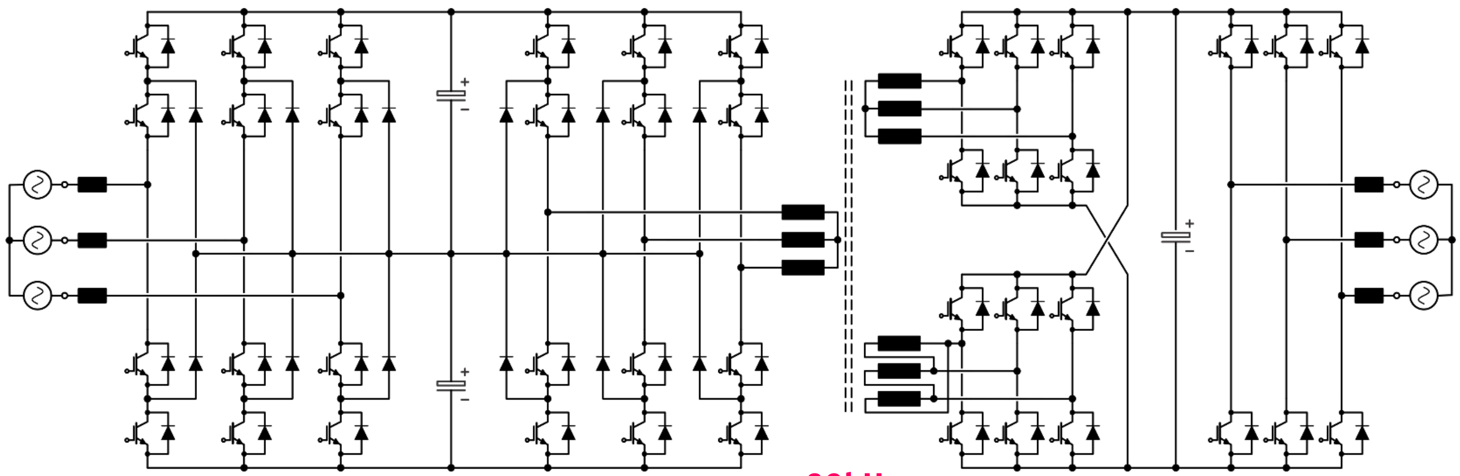




■ 1700V Power Semiconductors Best Suited for 10kV Mains → 10kV or Higher SiC Not Required (!)

▶ Single-Cell Structure

- 13.8kV → 480V
- Scaled Prototype
- 15kV SiC-IGBTs, 1200V SiC MOSFETs



- Redundancy Only for Series-Connection of Power Semiconductors (!)

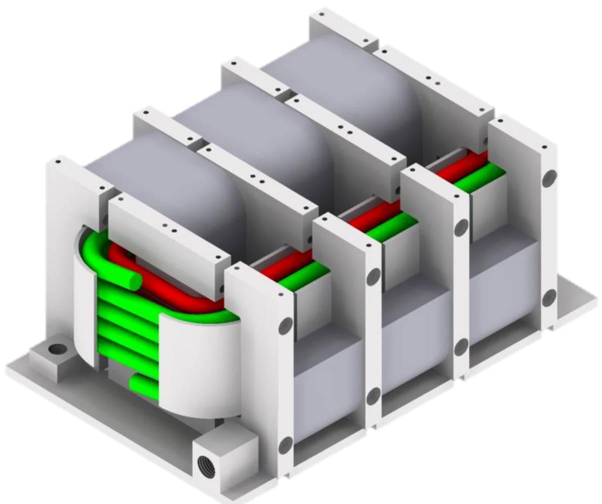
Challenge #3/5

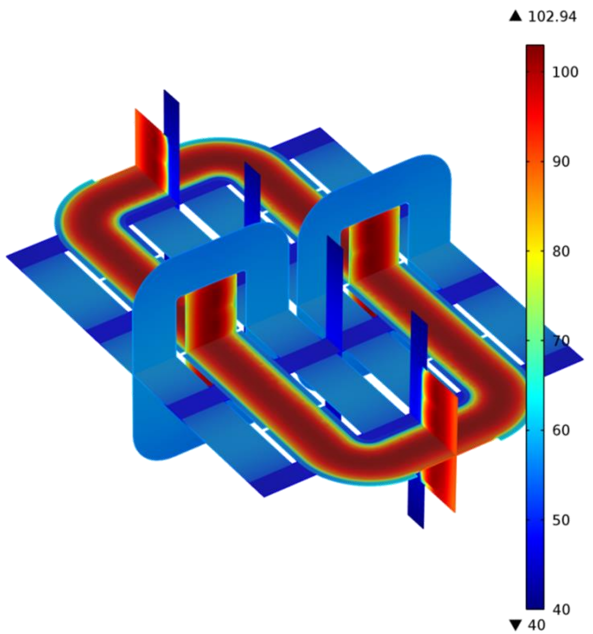
*Medium-Frequency
Transformer Design*

- *Heat Management*
- *Isolation*

▶ MF Transformer Design – Cold Plates/ Water Cooling

■ Nano-Crystalline 160kW/20kHz Transformer (ETH, Ortiz 2013)





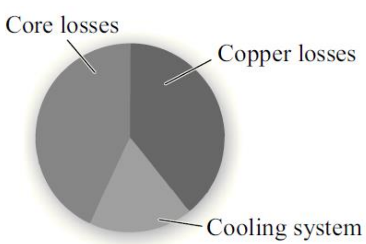
- Combination of Heat Conducting Plates and Top/Bottom Water-Cooled Cold Plates
- FEM Simulation Comprising Anisotropic Effects of Litz Wire and Tape-Wound Core

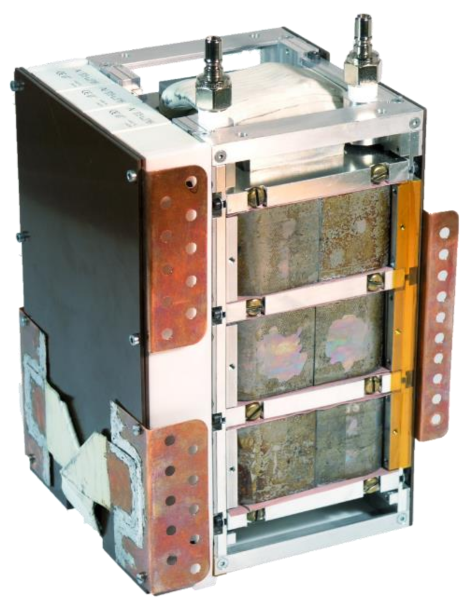
▶ Water-Cooled 20kHz Transformer

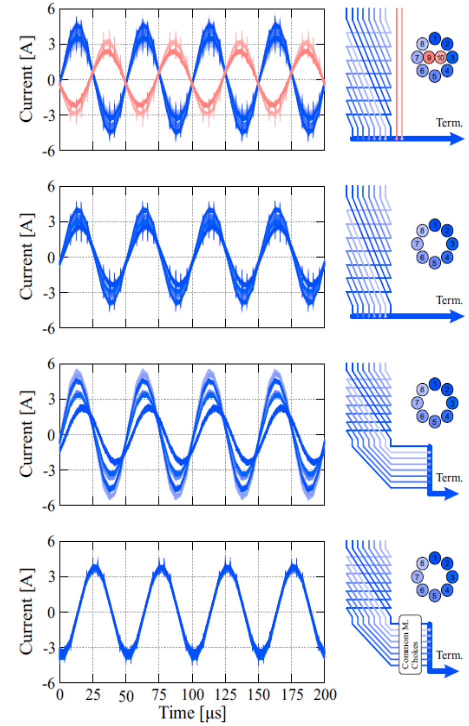
- Power Rating 166 kW
- Efficiency 99.5%
- Power Density 32 kW/dm³

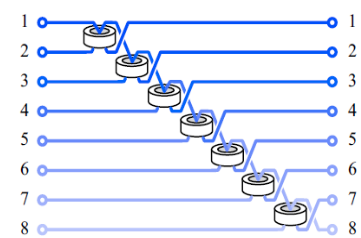
- Nanocrystalline Cores with 0.1mm Airgaps between Parallel Cores for Equal Flux Partitioning

- Litz Wire (10 Bundles) with CM Chokes for Equal Current Partitioning





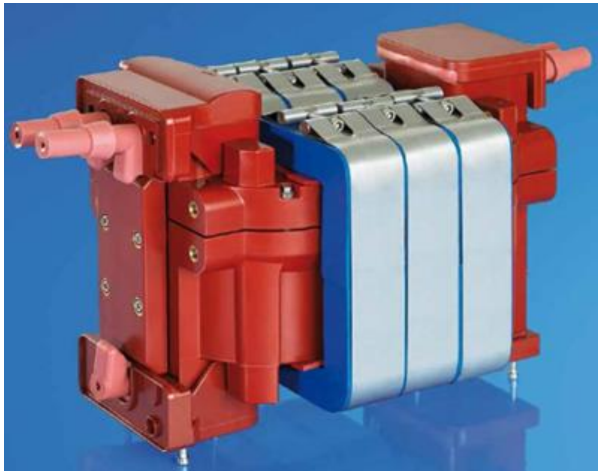




Further MF Transformer Examples

- Coaxial Windings – Shell Type
- Tunable Leakage Inductance
- Simple Terminations

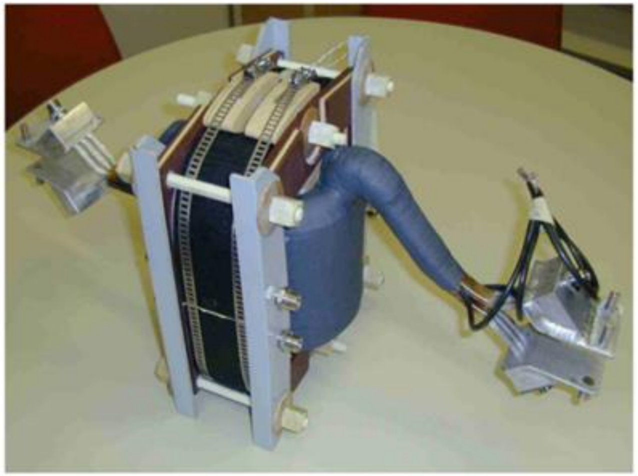
- 450kW @ 8 kHz / 50kg
- 99.7% Efficiency
- Dry Type / Liquid Isolation for 34.5kV



STS (2014)
www.sts-trafo.com

- 350kW @ 8 kHz
- Water Cooling / Hollow Conductors
- Isolation for 33kV

Steiner (2007)

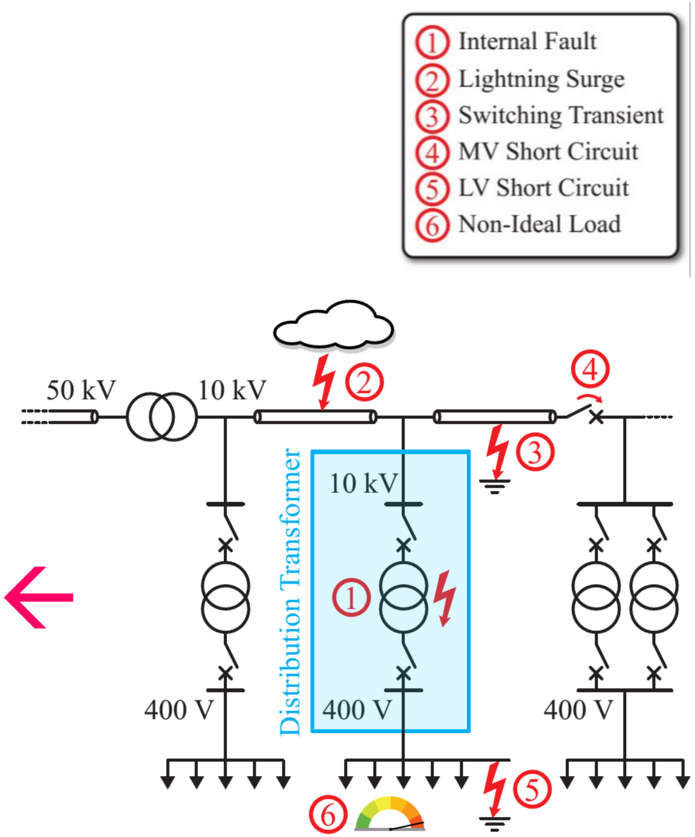


Challenge #4/5

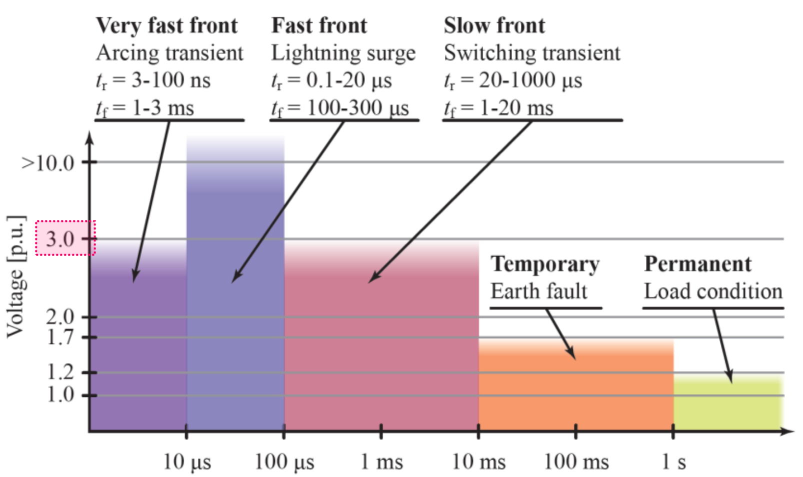
Mains ← SST → Load
Protection / Grid Codes

▶ Potential Faults of MV/LV Distribution-Type SSTs

- Extreme Overvoltage Stresses on the MV Side for Conv. Distr. Grids
- SST more Appropriate for Local Industrial MV Grids

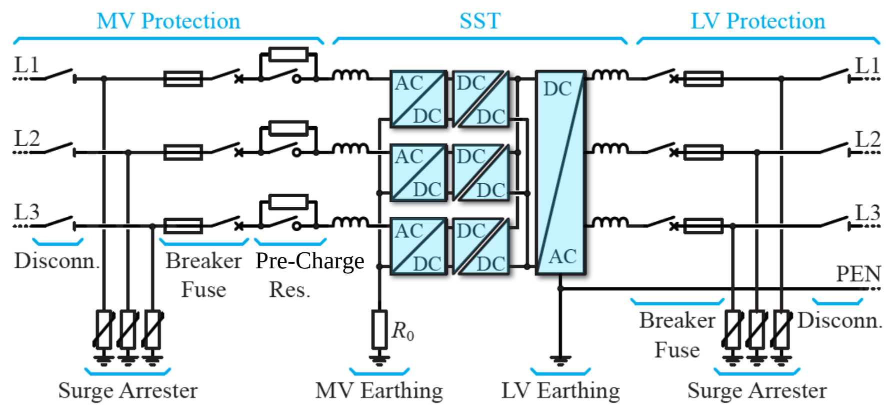


- Conv. MV Grid Time-Voltage Characteristic

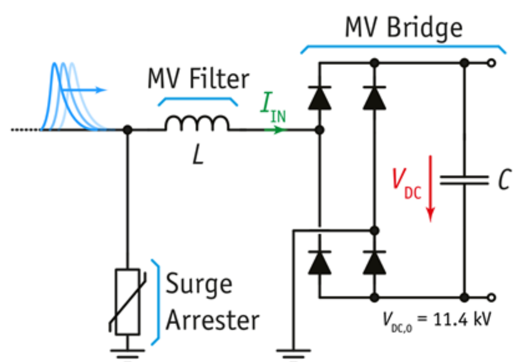


▶ Protection of LF-XFRM vs. SST Protection

■ Missing Analysis of SST Faults (Line-to-Line, Line-to-Gnd, S.C., etc.) and Protection Schemes



- Proposed SST Protection Scheme with Minimum # of Protection Devices

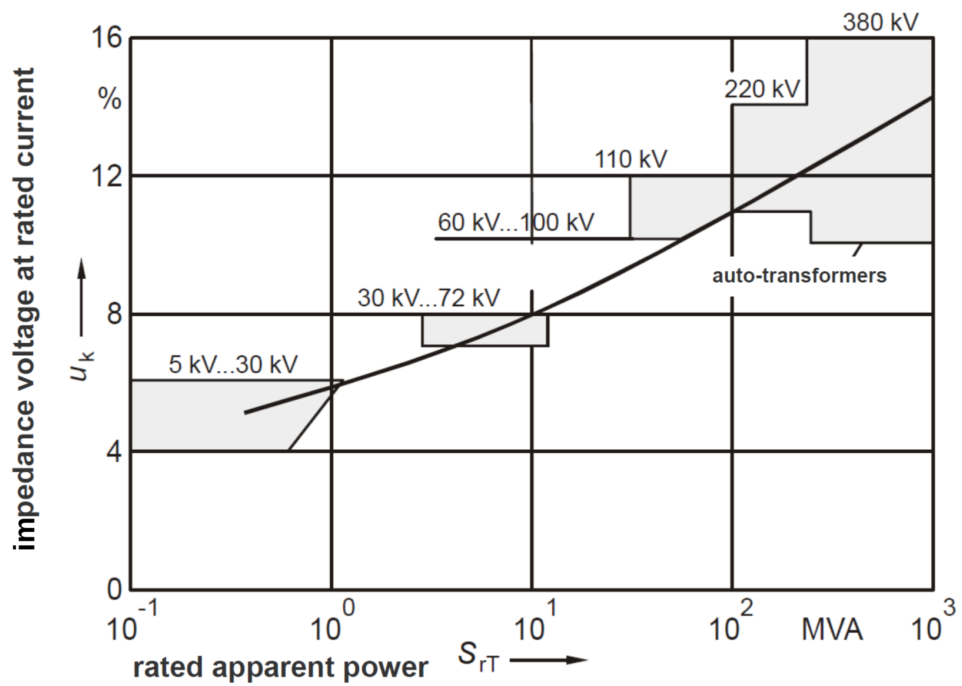


- Overvoltage Protection (Lightning Strike)
  * High Arrester Clamping Voltage
  * Filter Inductor > 8% for Current Limiting
  * Min. DC Link Capacitance
  * Sufficient Blocking Capability
  * Grounding – Lower Stress if Unearthed

■ Protection Scheme Needs to Consider: Selectivity / Sensitivity / Speed /Safety /Reliability

▶ Distribution Transformer Overcurrent Requirements

- Low-Frequ. XFRM must Provide Short-Circuit Currents of up to 40 Times Nominal Current for 1.5 Seconds (EWZ, 2009)
- Traction Transformers: 150% Nominal Power for 30 Seconds (Engel 2003)



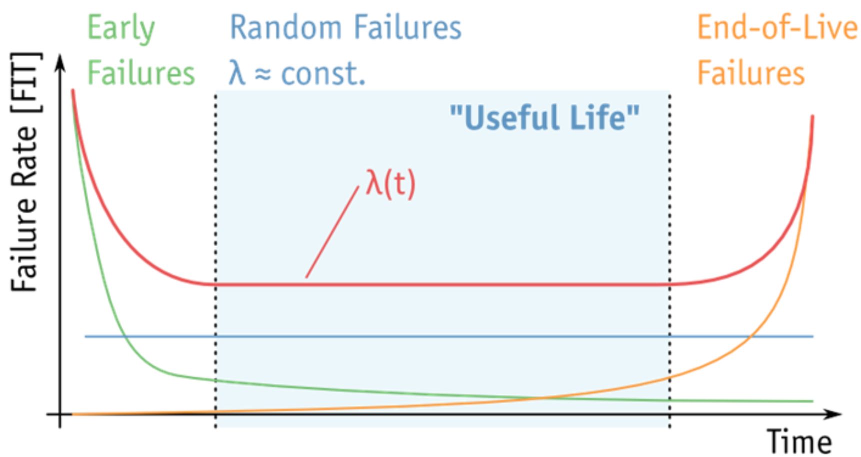
- Lower Grid Voltage Levels → Higher Relative Short Circuit Currents
- SST is NOT (!) a 1:1 Replacement for a Conventional Low-Frequency XFRM

Challenge #5/5

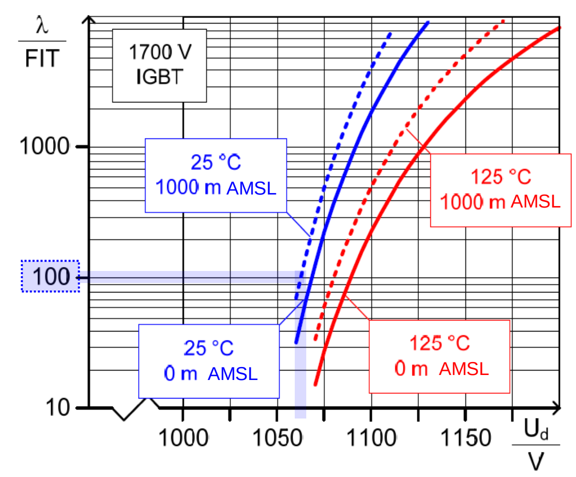
Ensuring Reliability of Highly Complex Multi-Cell Converter Topologies

▶ Reliability Model (1) – Failure Rate

- Failure Rate λ(t) is a Function of Time – „Bathtub Curve“
- Useful Life Dominated by Random Failures → λ(t) = const.
- [λ] = 1 FIT (1 Failure in 10^9 h)
- Typ. Value for IGBTs: 100 FIT



Source: H.-G. Eckel
Univ. Rostock



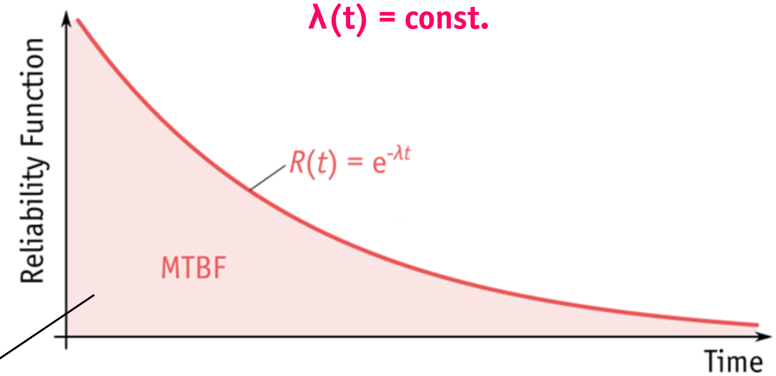
- Sources for Empirical Component Failure Rate Data : MIL-HDBK-217F, IEC Standard 62380, etc.

▶ Reliability Model (2) – Reliability Function

- **Reliability Function: Probability of System being Operational after *t*:**

$$R(t) = e^{-\int_0^t \lambda(x)dx} = e^{-\lambda t}$$

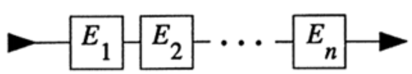
λ(t) = const.



- **Mean Time Between Failures**

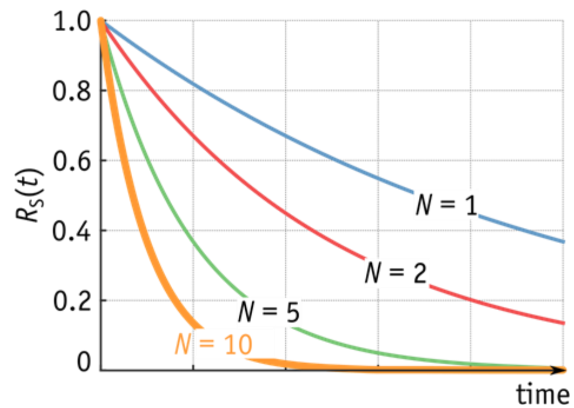
$$\text{MTBF} = \int_0^\infty R(t)dt = \int_0^\infty e^{-\lambda t}dt = \frac{1}{\lambda}$$

- **Series Structure**



$$\lambda_S = \sum_{i=1}^{n} \lambda_i$$

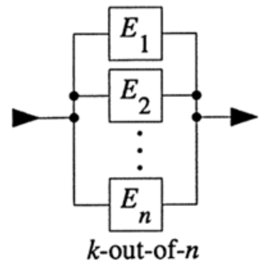
Independent Cells with Equal Failure Rate

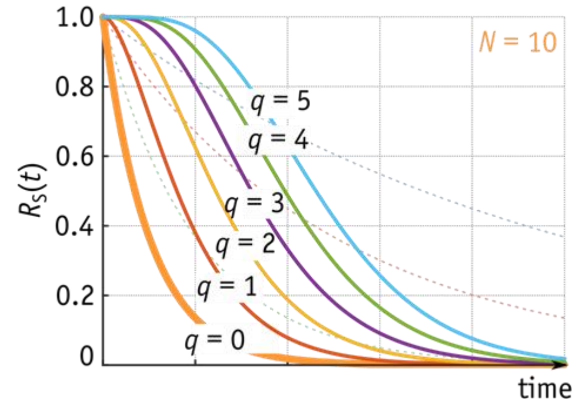


► Redundancy in Multi-Cell Converter Systems

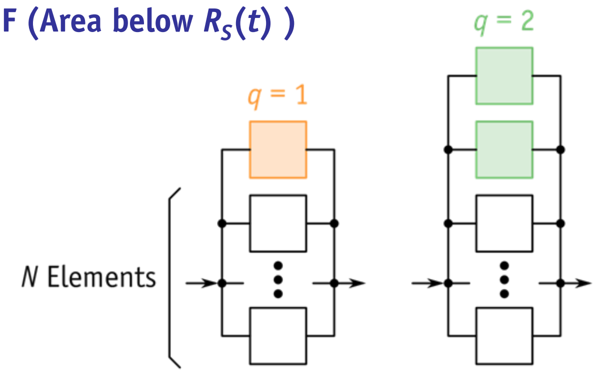
- ***k*-out-of-*n* Redundancy**
  Redundancy of Cells in Phase Stack

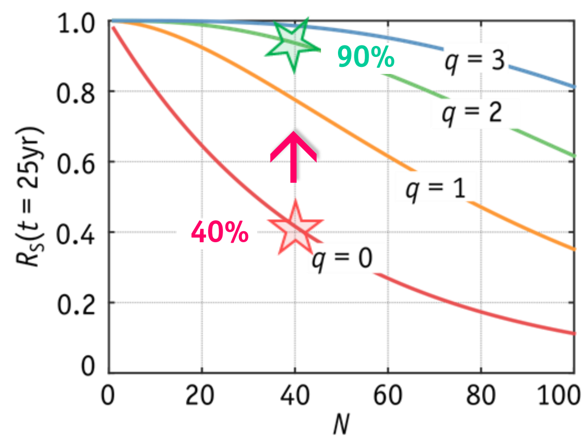
  ***System is Operational as Long as at Least k-out-of-n* Subsystems are Working**





- **Effect of *q* Redundant Cells on $R_S(t)$ and/or MTBF (Area below $R_S(t)$)**



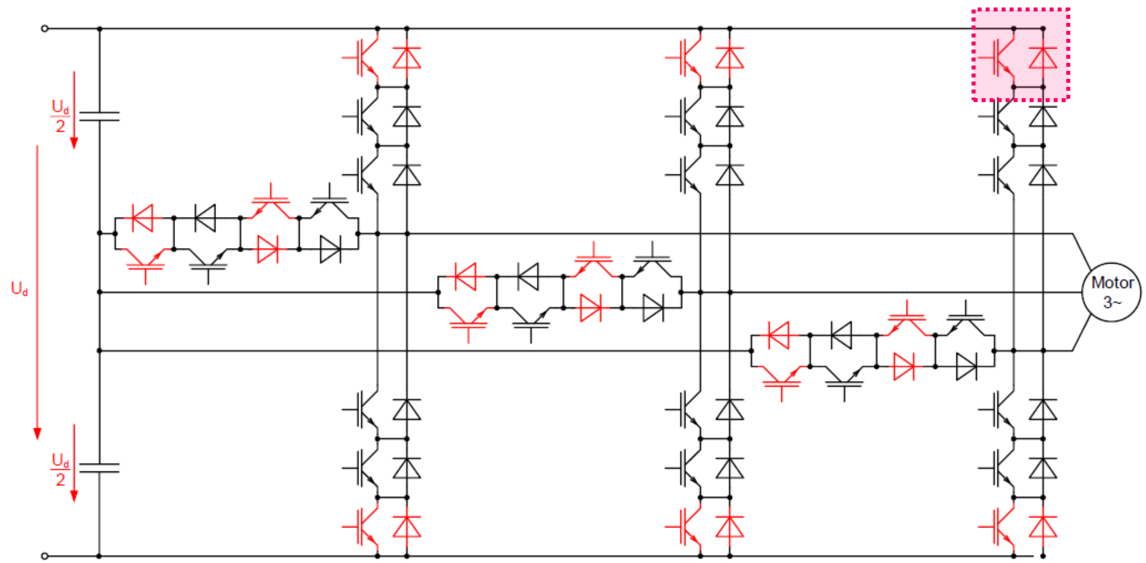


- **Redundancy Significantly Improves System Level Reliability (!)**

Redundancy in Single-Cell Converter Systems

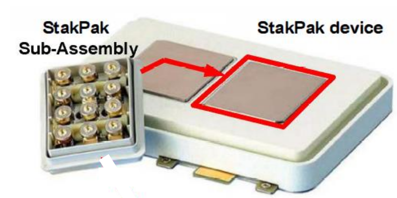
Source: M. Doppelbauer M. Hiller

- Example: Three-Level MV Motor Drive



- Redundant Series Device

Press-Pack NPC Phase Module



- Fail-to-Short Behavior Required (!)
- Only Feasible with Press-Pack Modules

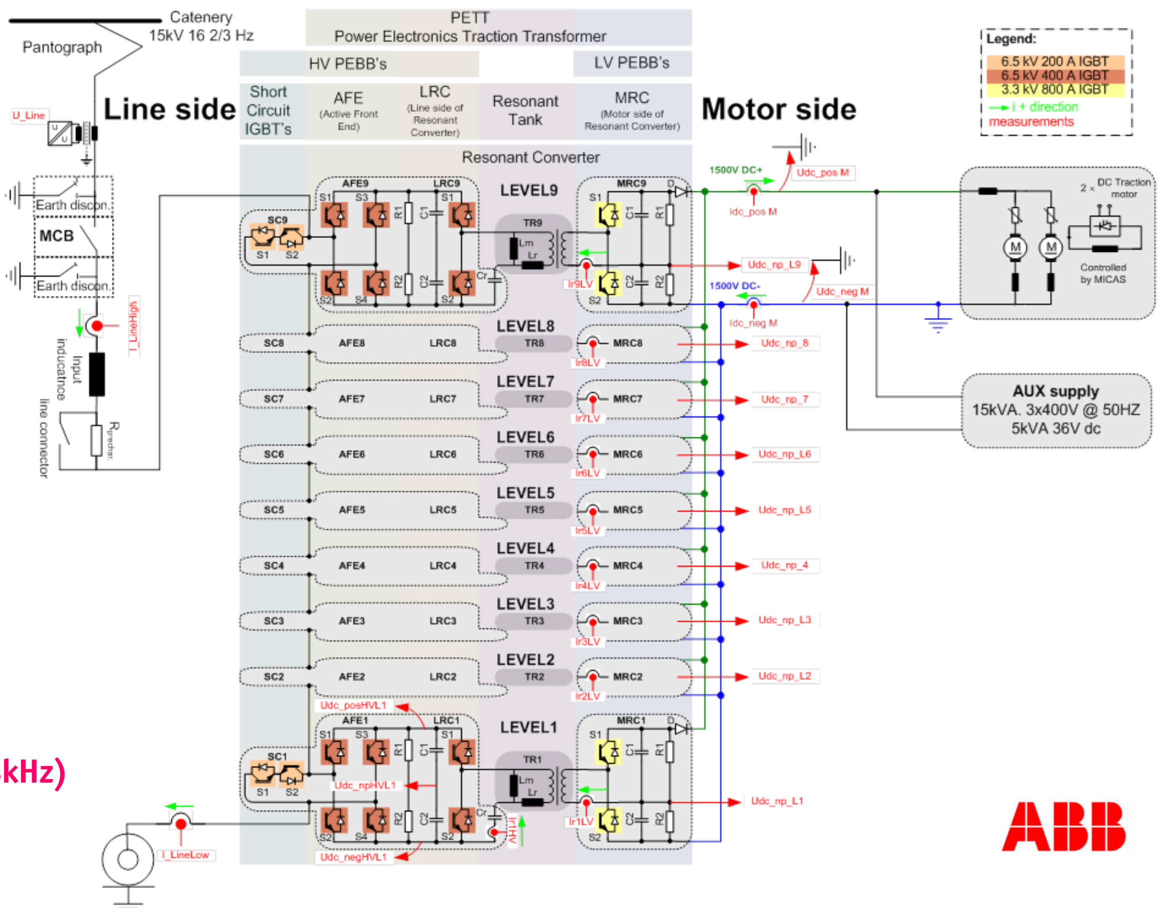
SST Demonstrator Systems

Future Locomotives
Smart Grid Applications

▶ 1ph. AC/DC Power Electronic Transformer - PET

- Dujic et al. (2011)

- Heinemann (2002)
- Steiner/Stemmler (1997)
- Schibli/Rufer (1996)



P = 1.2MVA, 1.8MVA pk
9 Cells (Modular)

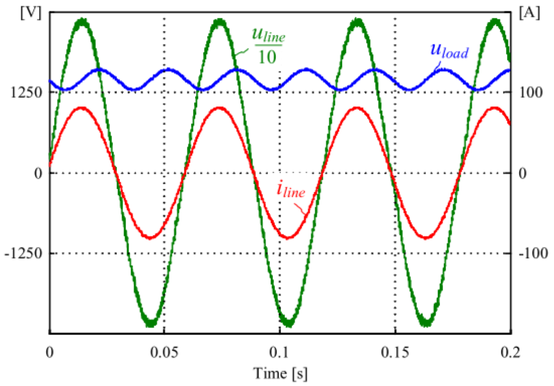
54 x (6.5kV, 400A IGBTs)
18 x (6.5kV, 200A IGBTs)
18 x (3.3kV, 800A IGBTs)

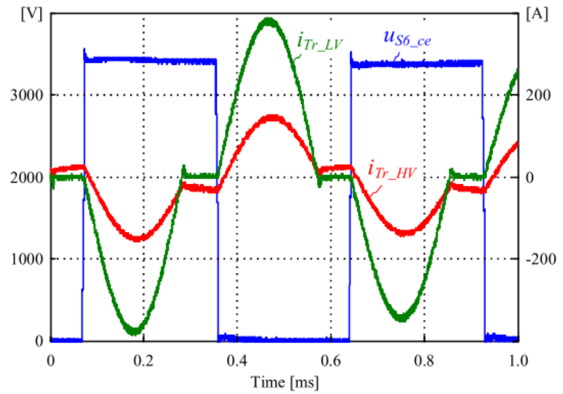
9 x MF Transf. (150kVA, 1.8kHz)
1 x Input Choke

ABB

▶ 1.2 MVA 1ph. AC/DC Power Electronic Transformer

- Cascaded H-Bridges – 9 Cells
- Resonant LLC DC/DC Converter Stages





▶ 1.2 MVA 1ph. AC/DC Power Electronic Transformer

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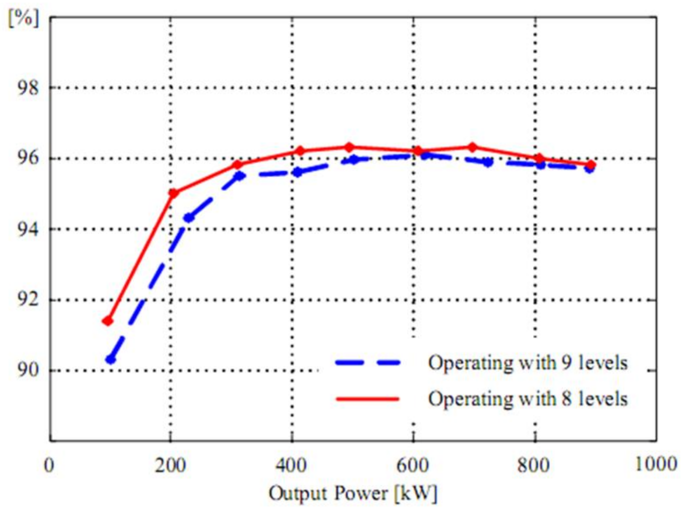
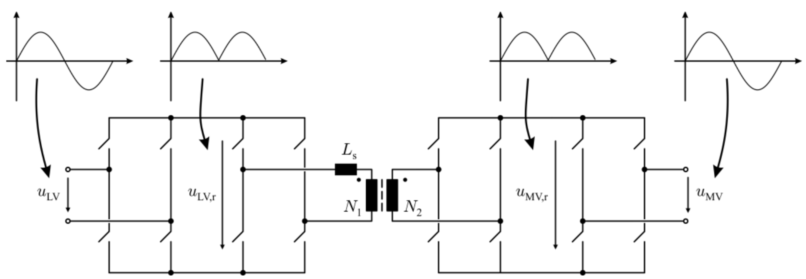
Efficiency

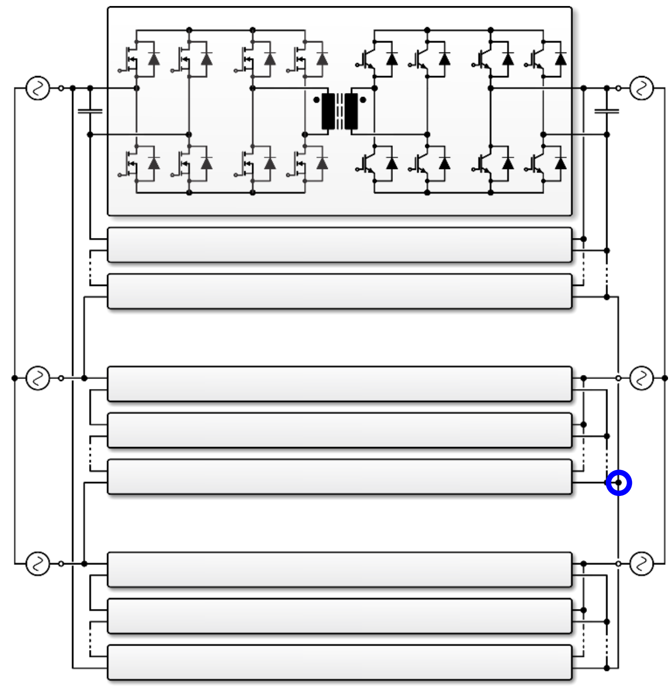


► SiC-Enabled Solid-State Power Substation

- Das et al. (2011)
- Lipo (2010)
- Weiss (1985 for Traction Appl.)

- Fully Phase Modular System
- Indirect Matrix Converter Modules ($f_1 = f_2$)
- MV Δ-Connection (13.8kV$_{l\text{-}l}$, 4 Modules in Series)
- LV Y-Connection (265V, Modules in Parallel)





- SiC Enabled 20kHz/1MVA "Solid State Power Substation"
- 97% Efficiency @ Full Load / 1/3rd Weight / 50% Volume Reduction (Comp. to 60Hz)

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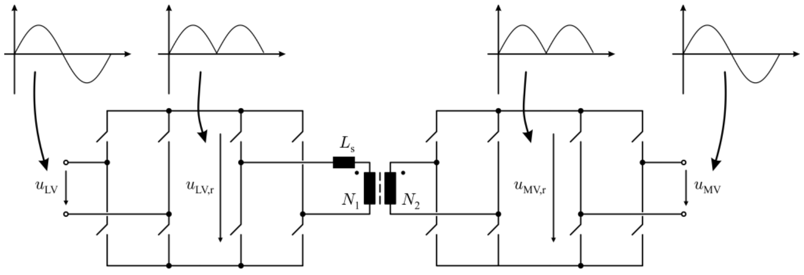


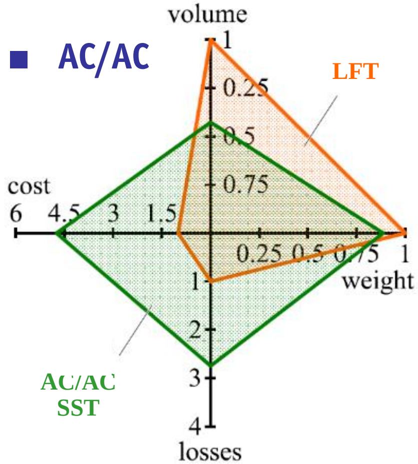
- SiC Enabled 20kHz/1MVA "Solid State Power Substation"
- 97% Efficiency @ Full Load / 1/3rd Weight / 50% Volume Reduction (Comp. to 60Hz)

▶ SST vs. LF Transformer + AC/AC or AC/DC Converter

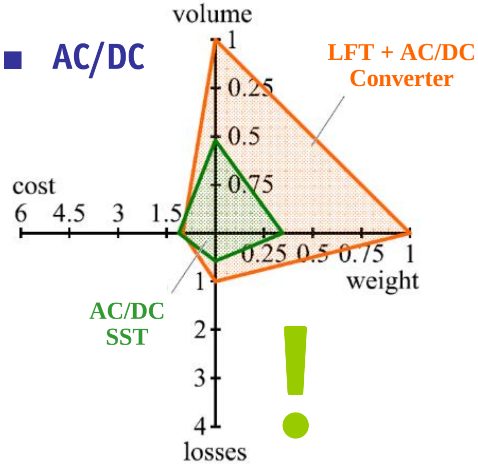
- Specifications
  1MVA
  10kV Input
  400V Output
  1700V IGBTs (1kHz/8kHz/4kHz)

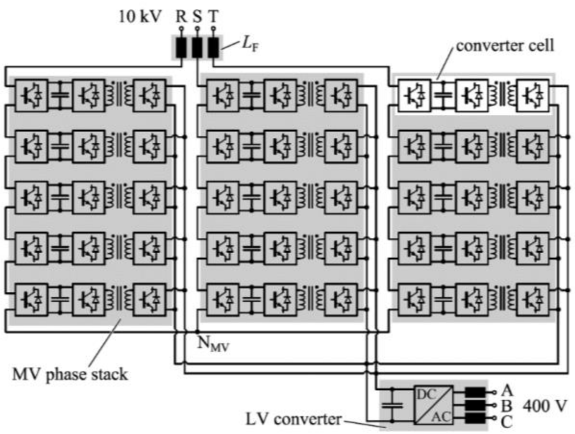
- LF Transformer
  98.7 %
  16.2 kUSD
  2600kg (5700lb)

■ AC/AC



■ AC/DC





- ■ Clear Efficiency/Volume/Weight Advantage of SST for DC Output (98.2%)
- ■ Weakness of AC/AC SST vs. Simple LF Transformer (98.7%) - 5 x Costs, 2.5 x Losses

Potential Future SST Application Areas

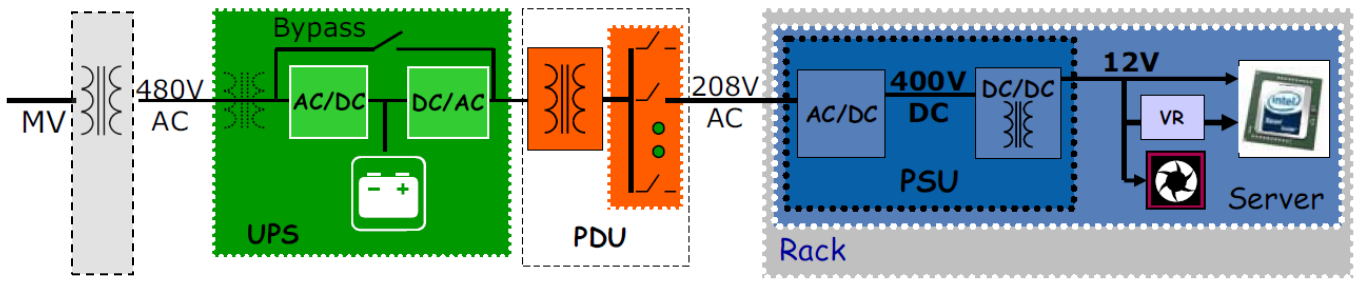
Datacenters
Off-Shore Wind
Oil and Gas Industry
Power-to-Gas
Distributed Propulsion Aircraft
More Electric Ships

▶ AC vs. Facility-Level DC Systems for Datacenters

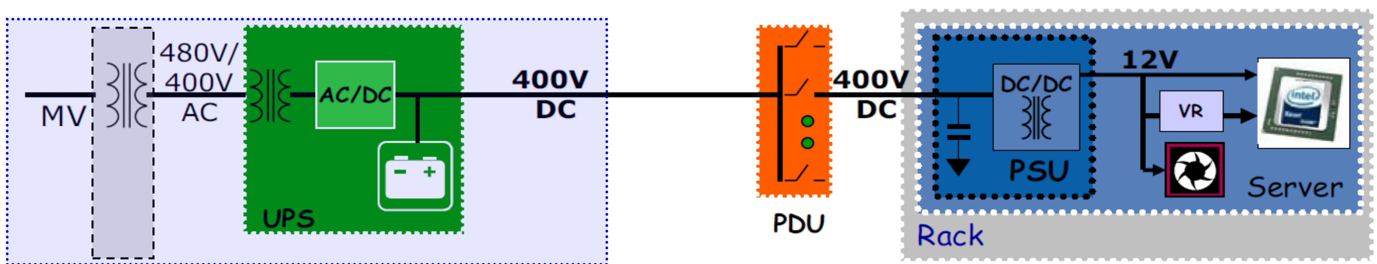
- Reduces Losses & Footprint
- Improves Reliability & Power Quality

— Conventional US 480V_{AC} Distribution

Source: intel 2007



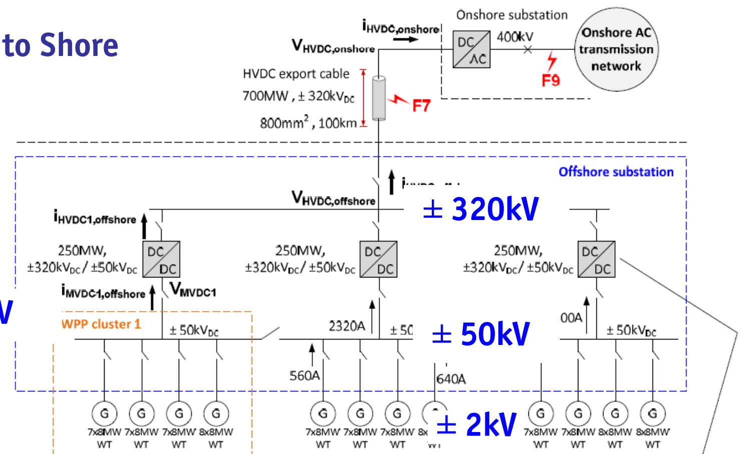
— Facility-Level 400 V_{DC} Distribution



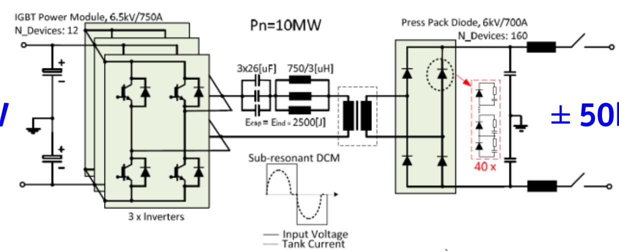
- Future Concept: Unidirectional SST / Direct 6.6kV AC → 400V DC Conversion

▶ DC Collection Grids for Offshore Wind Parks

- ± 320kV HVDC Transmission to Shore

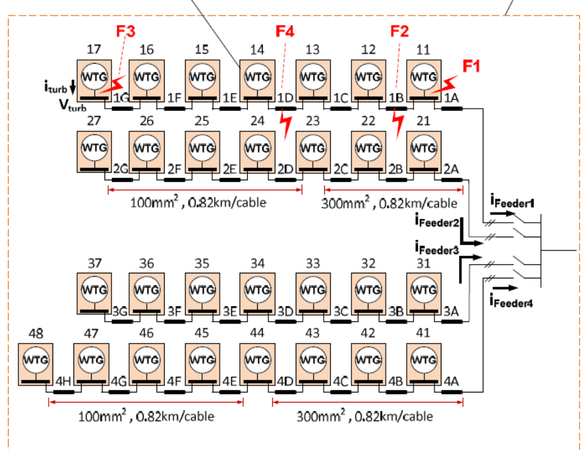


± 2kV

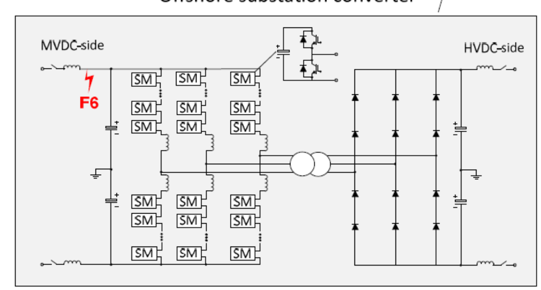


± 50kV

- **Unidirectional**
  Series Resonant
  MF DC→MVDC
  Conversion in each Wind Turbine



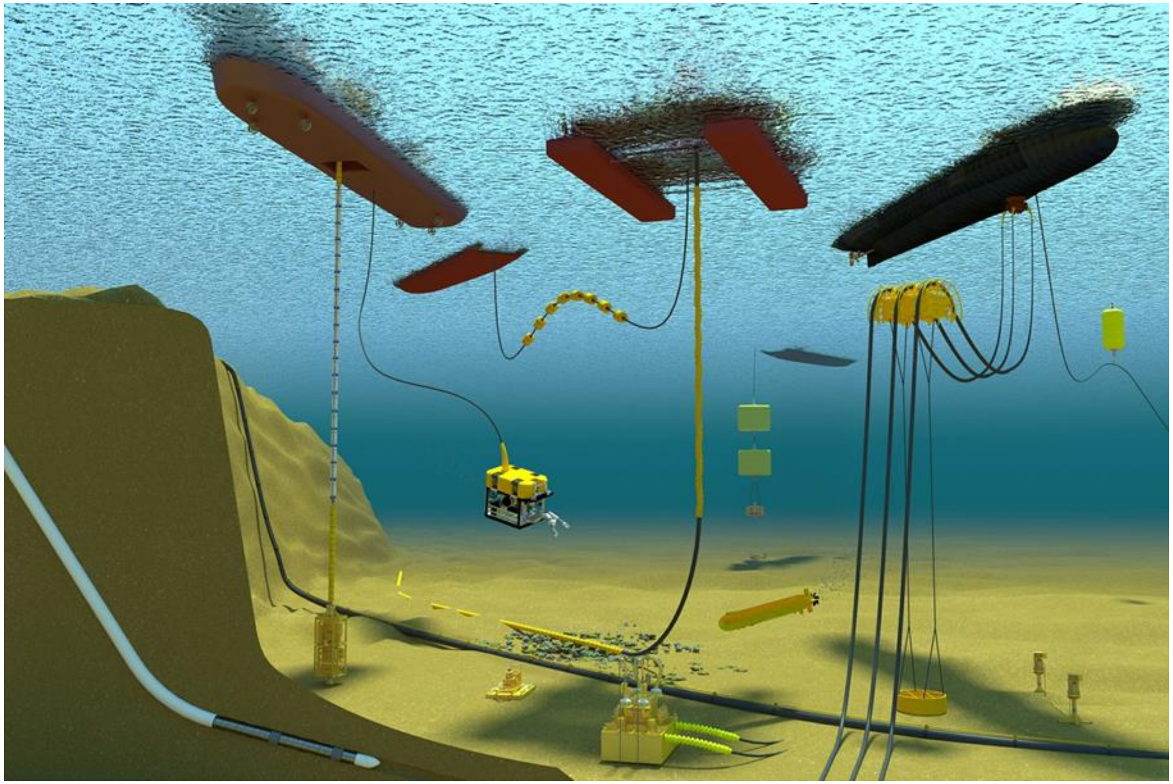
Offshore substation converter



- ± 50kV Offshore Collection Grid
- ± 50kV / ± 320kV Offshore Substation
- MMLC-Based MF Isolation

Source: Kjaer/2016

► Subsea Applications – Oil & Gas Processing



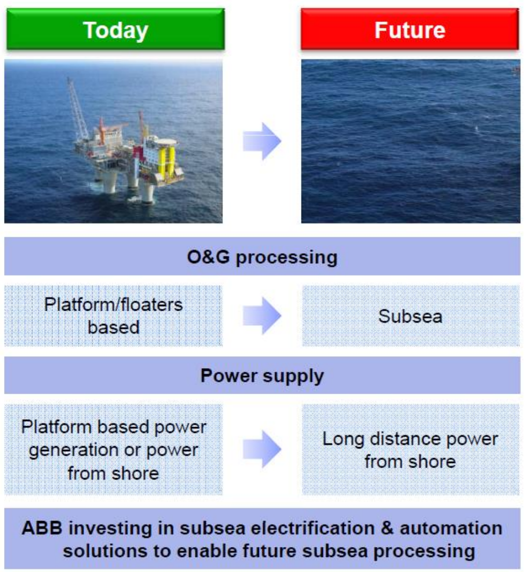
- ABB´s Future Subsea Power Grid → "Develop All Elements for a Subsea Factory"

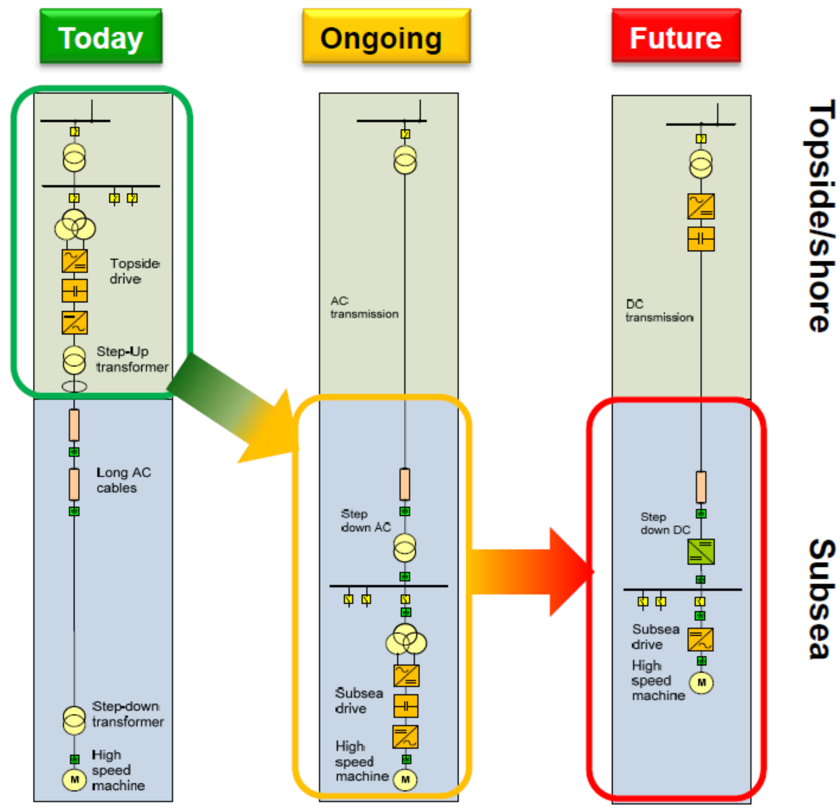
▶ Future Subsea Distribution Network

- Transmission Over DC, No Platforms/Floaters
- Longer Distances Possible
- Subsea O&G Processing

- Weight Optimized Power Electronics

Source: Devold (ABB 2012)

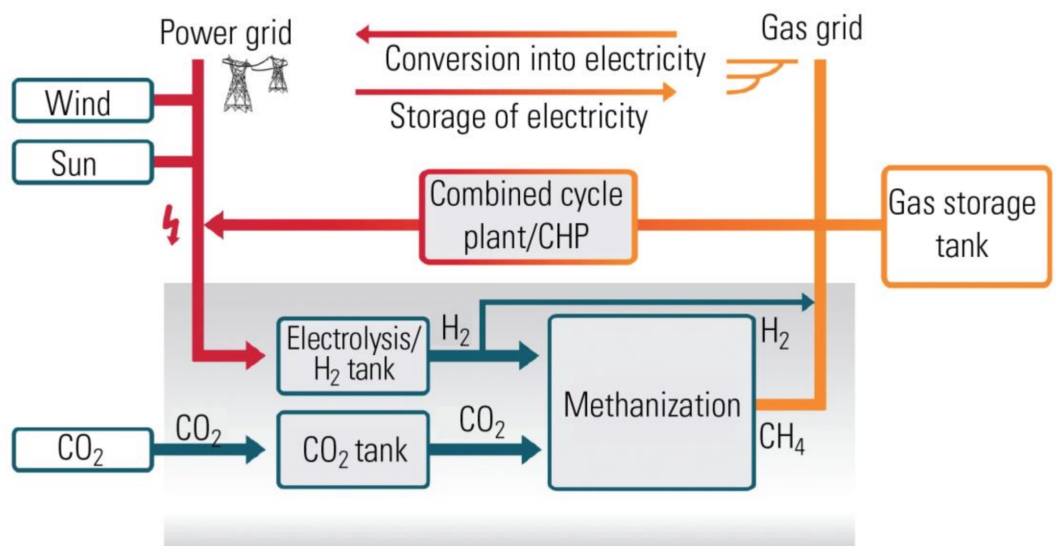




► Power-to-Gas

- Electrolysis for Conversion of Excess Wind/Solar Electric Energy into Hydrogen
  → Fuel-Cell Powered Cars
  → Heating

- High-Power @ Low DC Voltage (e.g. 220V)
- Very Well Suited for MV-Connected SST-Based Power Supply



– Hydrogenics 100 kW H_2-Generator (η=57%)

Source: www.r-e-a.net

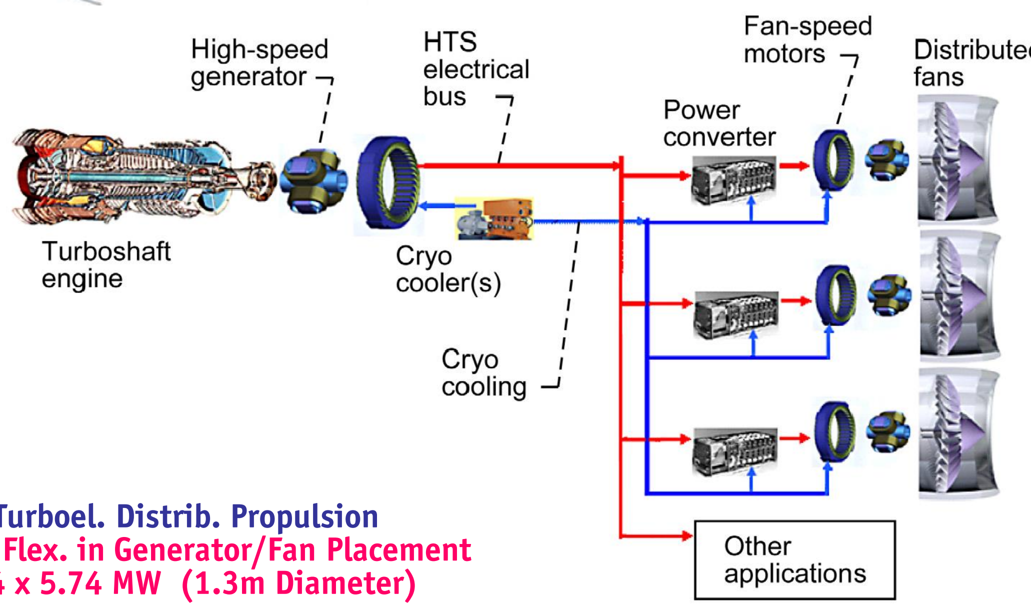
▶ Future Hybrid Distributed Propulsion Aircraft

Source: EADS

- Powered by Thermal Efficiency Optimized Gas Turbine and/or Future Batteries (1000 Wh/kg)
- Highly Efficient Superconducting Motors Driving Distributed Fans (E-Thrust)
- Until 2050: Cut CO_2 Emissions by 75%, NO_x by 90%, Noise Level by 65%

► Future Distributed Propulsion Aircraft

Source: NASA

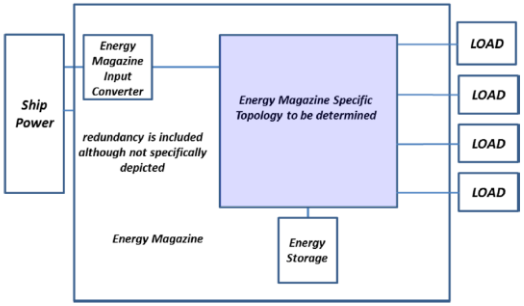


- NASA N3-X Vehicle Concept using Turboel. Distrib. Propulsion
- Electr. Power Transm. allows High Flex. in Generator/Fan Placement
- Generators: 2 x 40.2MW / Fans: 14 x 5.74 MW (1.3m Diameter)

Future Naval Applications

- MV Cellular DC Power Distribution on Future Combat Ships etc.

Source:
General Dynamics



- "Energy Magazine" as Extension of Electric Power System / Individual Load Power Conditioning
- Bidirectional Power Flow for Advanced Weapon Load Demand
- Extreme Energy and Power Density Requirements

Future Naval Applications

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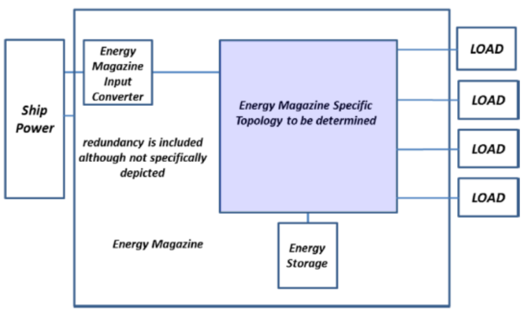
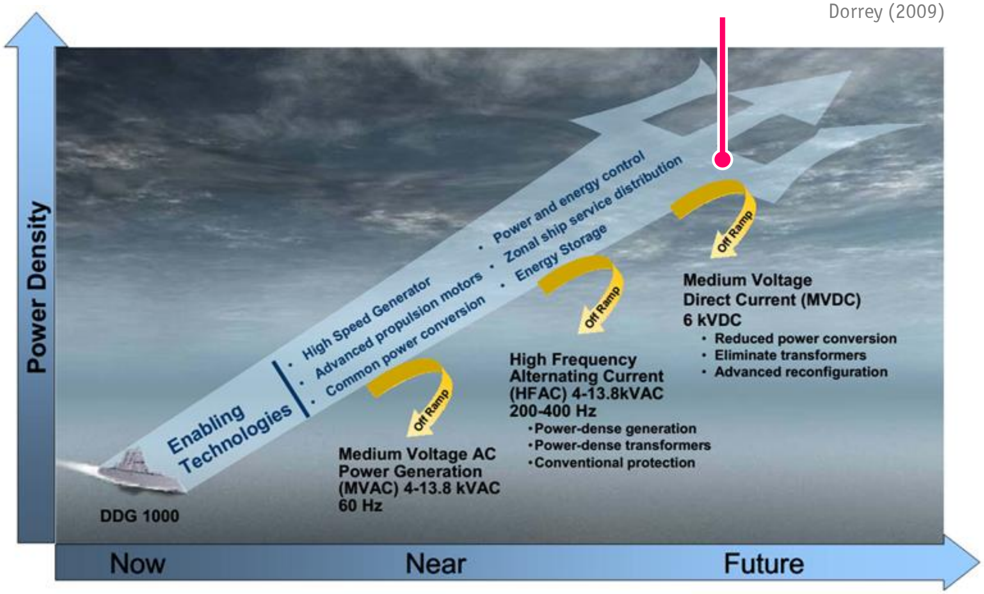
6kV DC/DC SST for Size/Weight Reduction

Dorrey (2009)





- "Energy Magazine" as Extension of Electric Power System / Individual Load Power Conditioning
- Bidirectional Power Flow for Advanced Weapon Load Demand
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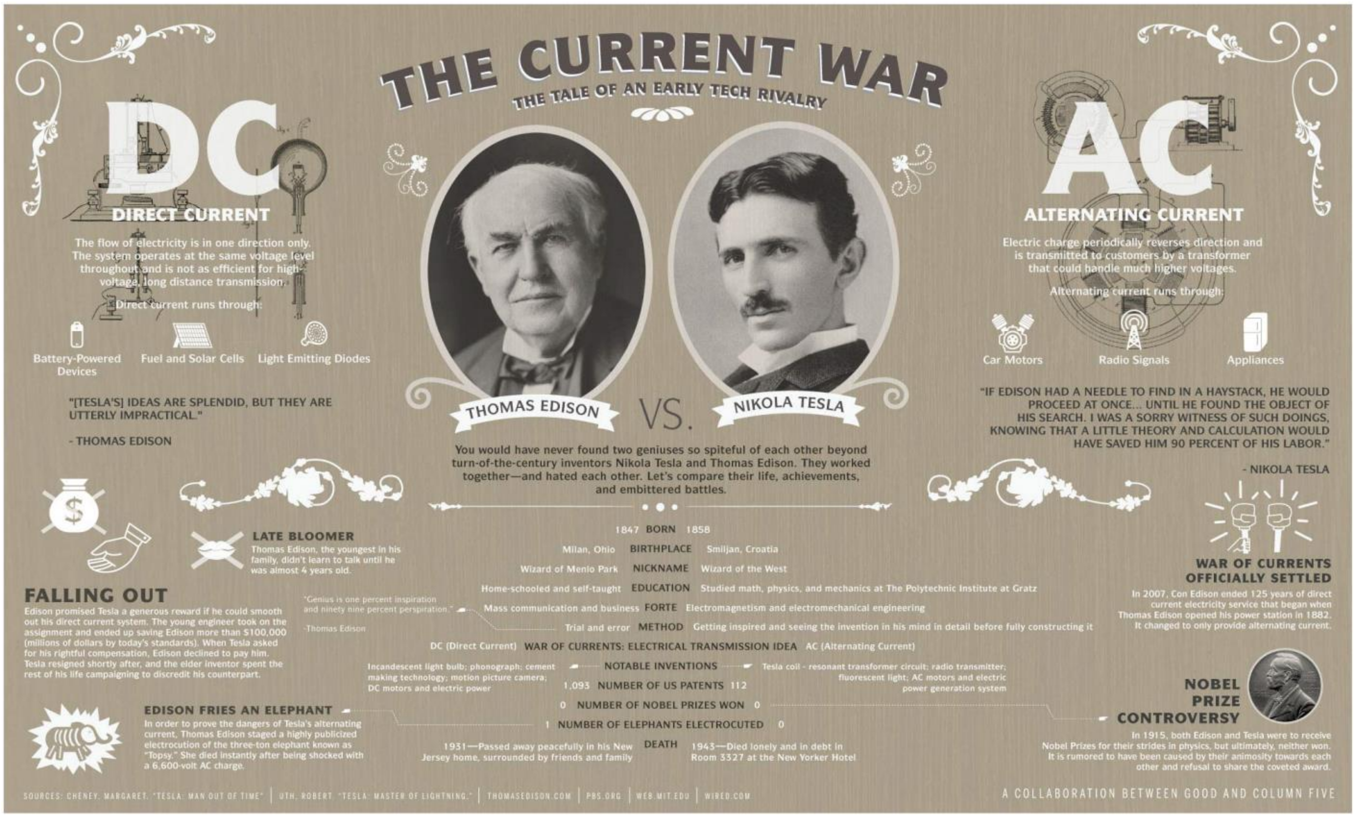
Conclusions

SST Limitations / Concepts
Research Areas

► SST Ends the "War of Currents"



- No "Revenge" of T.A. Edison but Future "Synergy" of AC and DC Systems !

SST Applications - The Road Ahead

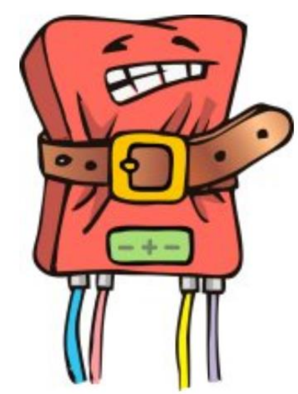
- NOT (!) Weight / Space Limited
- Smart Grid, Stationary Applications

- AC/AC
  - Efficiency Challenge
  - Controllability also by More Efficient Alternatives
    - * Tap Changers
    - * Series Regulators (Partial Power Processing)
  - Not Compatible w. Existing Infrastr.
  - Cost / Robustness / Reliability

- AC/DC
  - Efficiency Challenge more Balanced
  - "Local" Applic. (Datacenters, DC Distr.)
  - Cost / Robustness / Reliability

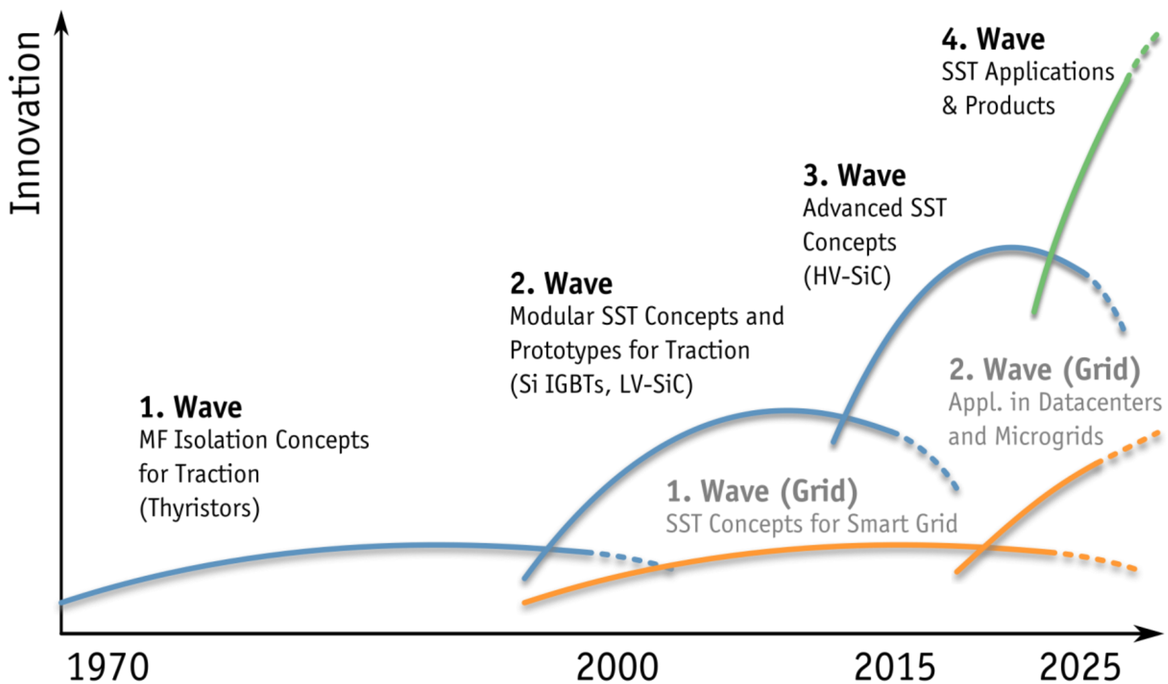
- DC/DC
  - No Other Option (!)
  - MV DC Collection Grids (Wind, PV)
  - Sw. Frequ. as DOF of Design

- Weight / Space Limited
- Traction Applic. etc.



- DC/DC
- AC/DC
- AC/AC
  - Sw. Frequ. as DOF of Design
  - Low Weight/Volume @ High Eff.
  - Local Applic. (Load/Source Integr.)

► SST Development Cycles - Outlook



- **Development Reaching Over Decades – Matched to "Product" Life Cycle**

Thank You!

Questions