

Source:
next-gen-
forum.com

NEXT SiC/GaN 3- Φ Variable GEN^{ERATION} Speed Drive Systems

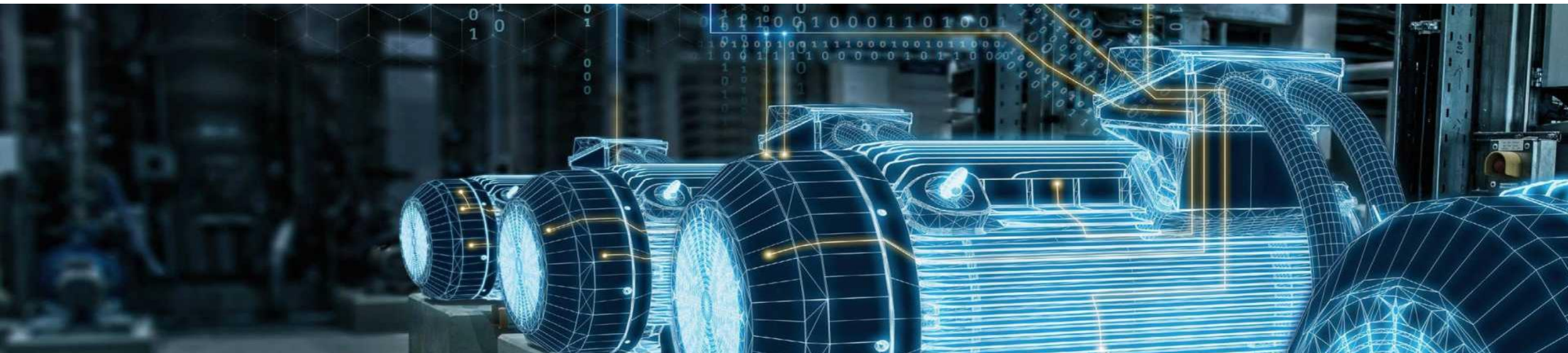
Johann W. Kolar et al.



Swiss Federal Institute of Technology (ETH) Zurich
Power Electronic Systems Laboratory
www.pes.ee.ethz.ch

Nov. 11, 2024

Source: SIEMENS



... *“How to Handle a Double-Edged Sword”?*

Johann W. Kolar | Jonas Huber



Swiss Federal Institute of Technology (ETH) Zurich
Power Electronic Systems Laboratory
www.pes.ee.ethz.ch

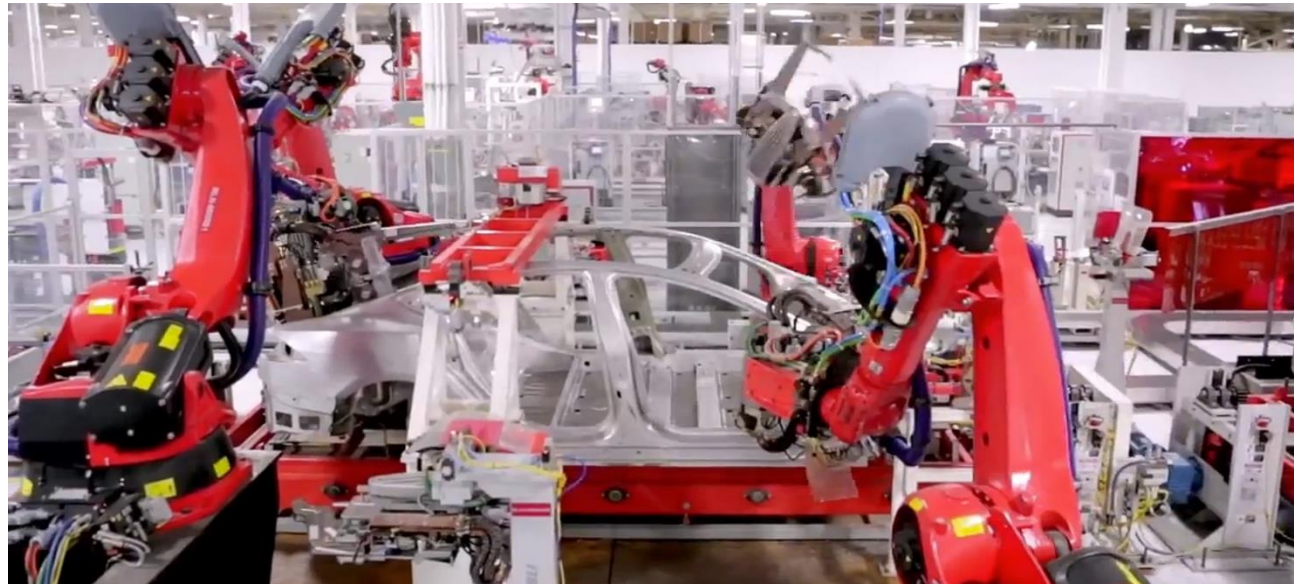
Nov. 11, 2024



Variable Speed Motor Drive (VSD) Systems

- *Industry Automation / Robotics*
- *Material Machining / Processing – Drilling, Milling, etc.*
- *Compressors / Pumps / Fans*
- *Transportation*
- *etc., etc.*

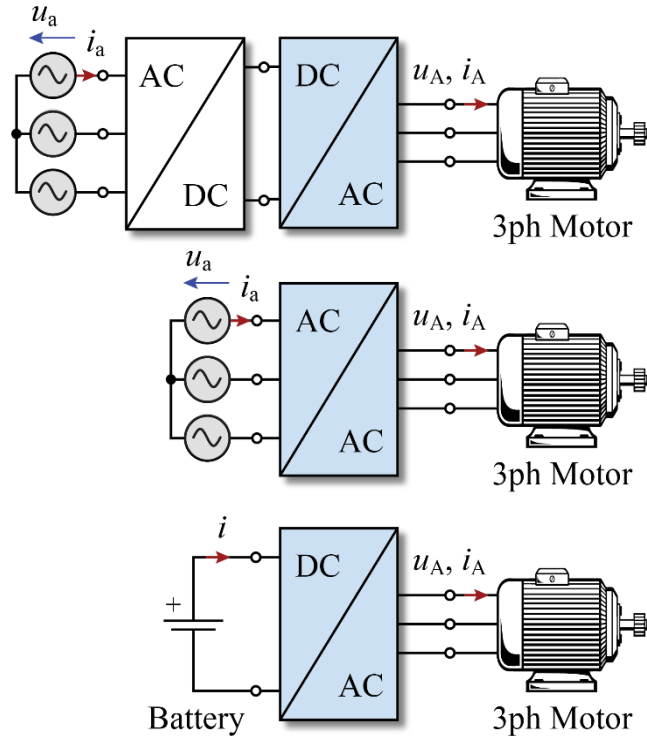
.... Everywhere !



- *60...70 % of All Electric Energy Used in Industry Converted by VSDs*

Variable Speed Drives — State-of-the-Art 1/2

- *DC-Link Based AC/DC/AC OR Matrix-Type AC/AC Converters*
- *Battery OR Fuel-Cell Supply OR Common DC-Bus Concepts*



38%
of electric energy use is for motors in commercial buildings.



70%
of electricity consumed by industry is used in electric motor systems.

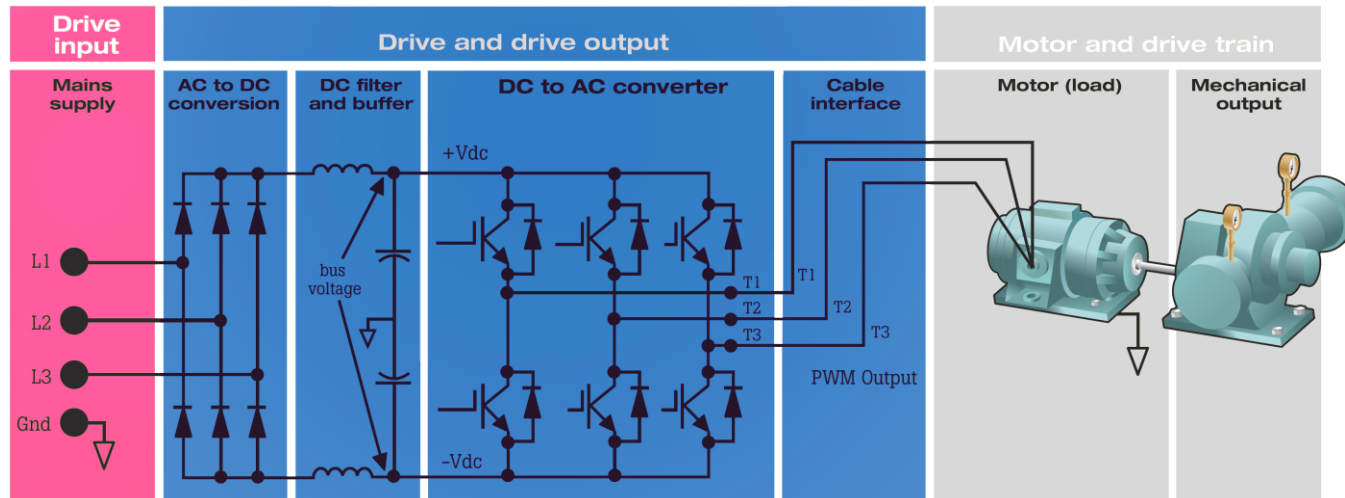
Source: **ABB**

- *45% of World's Electricity Used for Motors in Buildings & Industrial Applications*

Variable Speed Drives — State-of-the-Art 2/2

- *Mains Interface | 3-Φ PWM Inverter | Cable | Motor → All Separated*
- *PWM Output → Conducted & Radiated EMI / Reflections @ Motor Terminals / Bearing Currents*
- *Large Installation Space* / \$\$\$
- *Shielded Motor Cables / Filters* / \$\$\$
- *Special Types of Bearings / Grounding* / \$\$\$
- *Complicated / Expert Installation* / \$\$\$

Source: FLUKE



- *High Performance @ High Level of Complexity & High Costs (!)*

SiC Low $R_{DS(on)}$ High-Voltage Devices

- Higher Critical E-Field of SiC → Thinner Drift Layer
- Higher Maximum Junction Temperature $T_{j,max}$

at 300 K	Si	GaAs	4H/6H-SiC	GaN
E_g (eV)	1.12	1.4	3.0-3.2	3.4
E_c (MV/cm)	0.25	0.3	2.2-2.5	3
μ_n (cm ² /Vs)	1350	8500	100-1000	1000
ϵ_r	11.9	13	10	9.5
v_{sat} (cm/s)	1×10^7	1×10^7	2×10^7	3×10^7
λ (W/cmK)	1.5	0.5	3 - 5	1.3

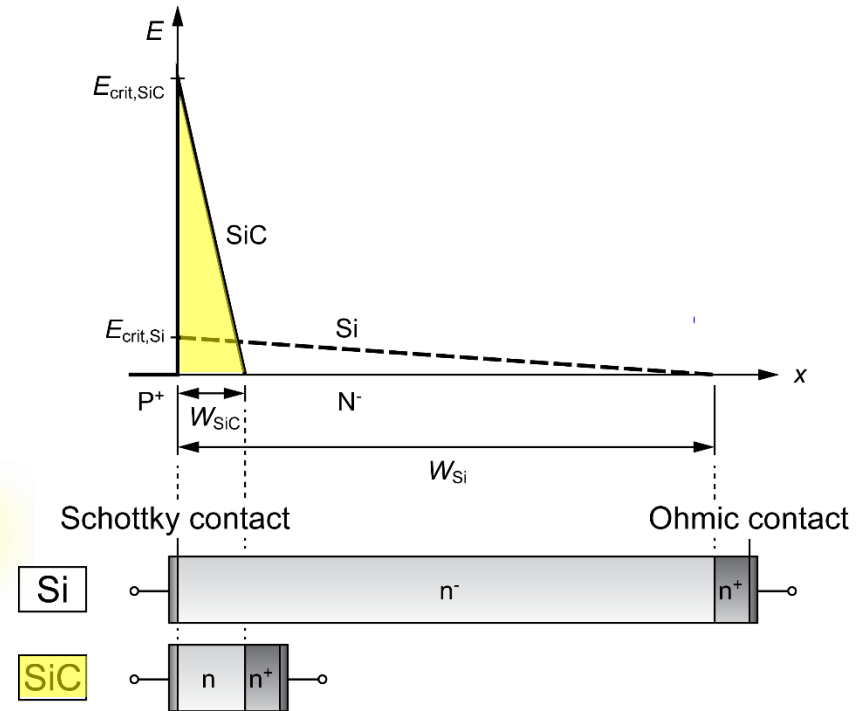
© 2000 Carl-Mikael Zetterling

$$R_{on}^* = \frac{4V_B^2}{\epsilon\mu_n E_C^3} \leftarrow$$

For 1kV:

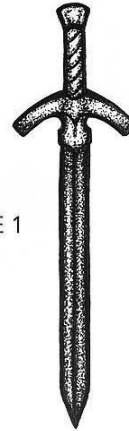
	Si	SiC
W (μm)	100	10
N_D (cm ⁻³)	10^{14}	10^{16}

$$R_{on,SiC}^* \approx \frac{1}{300} R_{on,Si}^*$$



- Massive Reduction of Relative On-Resistance → High Blocking Voltage Unipolar (!) Devices

— *Advantages* —

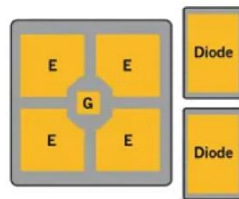
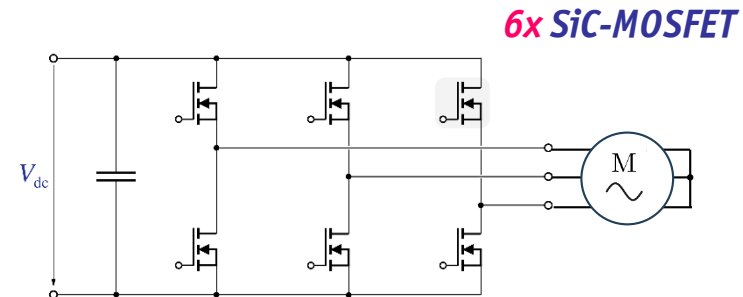
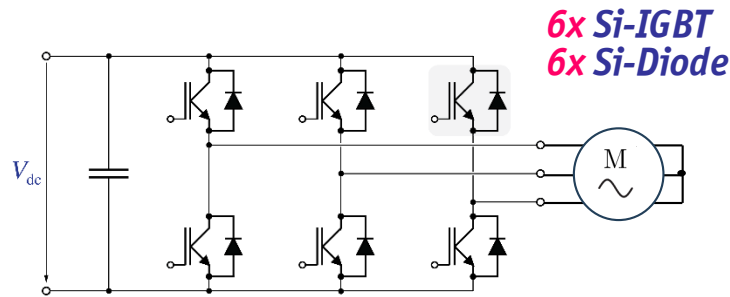


EDGE 1

EDGE 2

Si vs. SiC

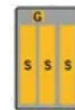
- **Si-IGBT / Diode** → *Const. On-State Voltage, Turn-Off Tail Current & Diode Reverse Recovery Current*
- **SiC-MOSFET** → *Loss Reduction @ Part Load BUT Higher R_{th}*



1200V 100A
Die Size: 98.8mm² + 39.4mm²

Source: Infineon

Source: ATZ elektronik



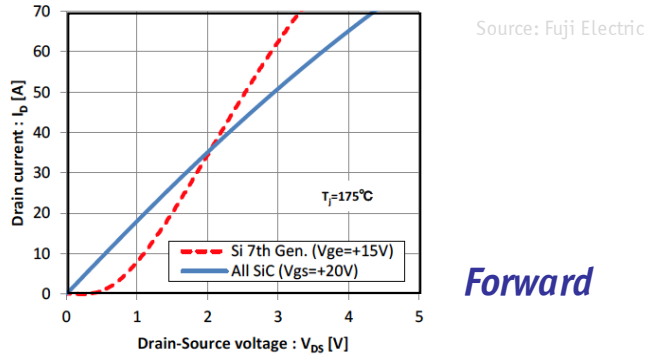
1200V 100A
Die Size: 25.6mm²

Source: Cree

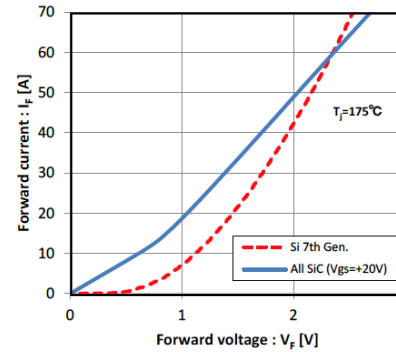
- **Space Saving of >30% on Module Level (!)**

Si vs. SiC Conduction Behavior

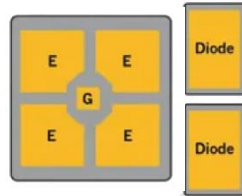
- **Si-IGBT** → **Const. On-State Voltage Drop / Rel. Low Switching Speed**
- **SiC-MOSFETs** → **Resistive On-State Behavior / Factor 10 Higher Sw. Speed**



Forward

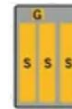


Reverse



1200V 100A
Die Size: 98.8mm² + 39.4mm²

Source: Infineon



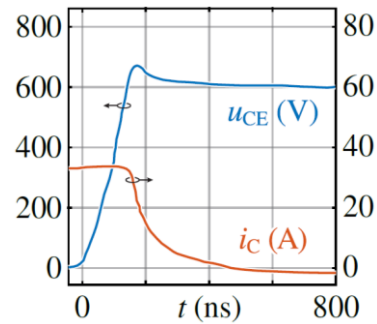
1200V 100A
Die Size: 25.6mm²

Source: Cree

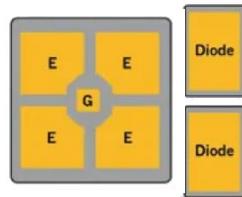
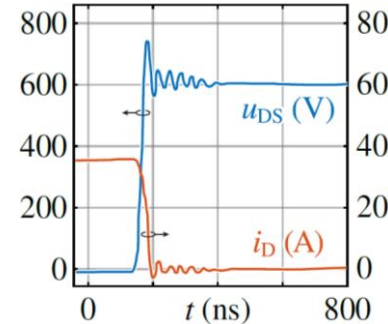
- **SiC MOSFETs Facilitate Higher Part Load Efficiency**

Si vs. SiC Switching Behavior

- **Si-IGBT** → *Const. On-State Voltage Drop / Rel. Low Switching Speed*
- **SiC-MOSFETs** → *Resistive On-State Behavior / Factor 10 Higher Sw. Speed*

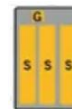


Source: Fuji Electric



1200V 100A
Die Size: 98.8mm² + 39.4mm²

Source: Infineon

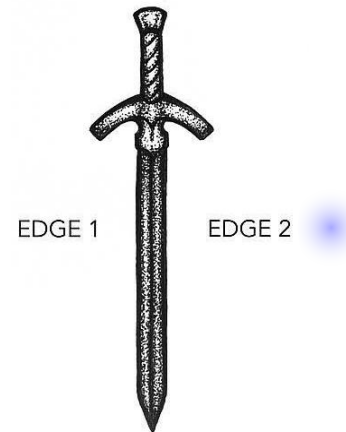


1200V 100A
Die Size: 25.6mm²

Source: Cree

- **High di/dt & dv/dt** → *Challenges in Packaging / EMI / Motor Insulation / Bearing Currents*

— *Challenges* —

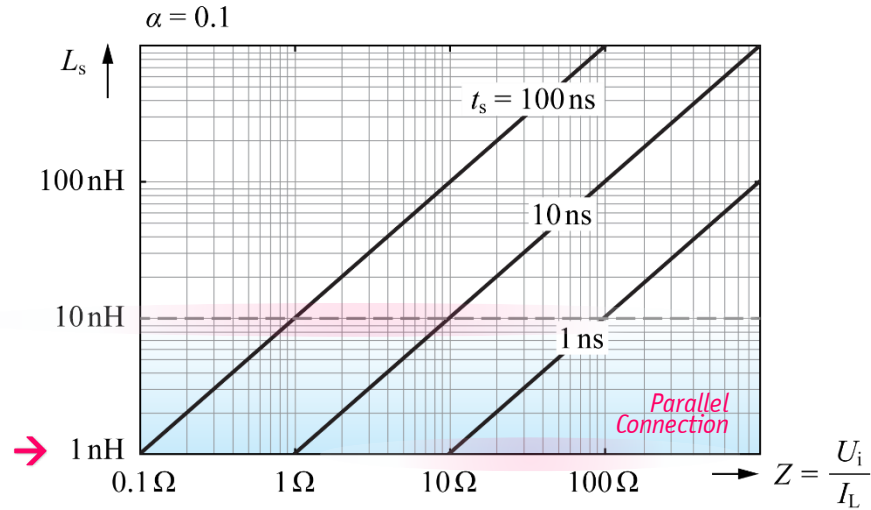
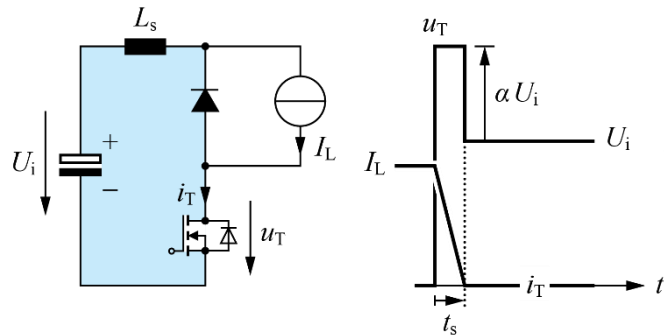


Low Commutation Loop Inductance

- High di/dt Switching Transition
- Commutation Loop Inductance L_s
- Allowed L_s Directly Related to Switching Time t_s →

$$L \frac{di}{dt} = u$$

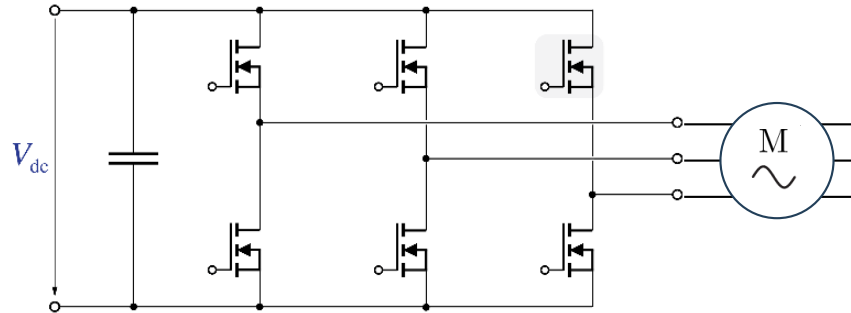
$$L_s \leq \frac{\alpha U_i}{\frac{I_L}{t_s}} = \alpha t_s \frac{U_i}{I_L}$$



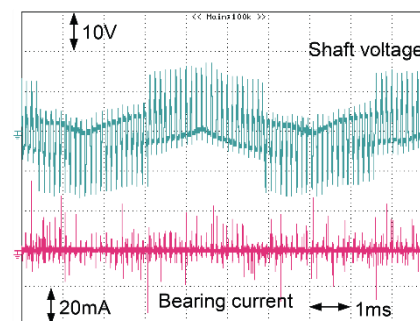
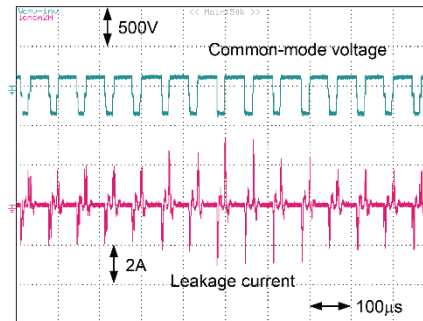
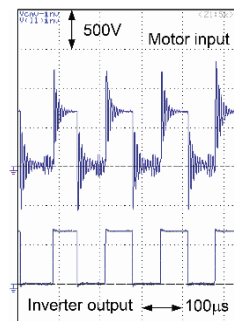
- **Advanced Packaging & Parallel Interleaving for Partitioning of Large Currents (Z-Matching)**

Surge Voltage Reflections & CM Currents

- *High dv/dt / Short Rise Times of Inverter DM & CM Output Voltage Pulses*
- *Reflections @ Motor Terminals \rightarrow High Insulation Stress*
- *CM Leakage Current \rightarrow Radiated Emissions & Bearing Currents*



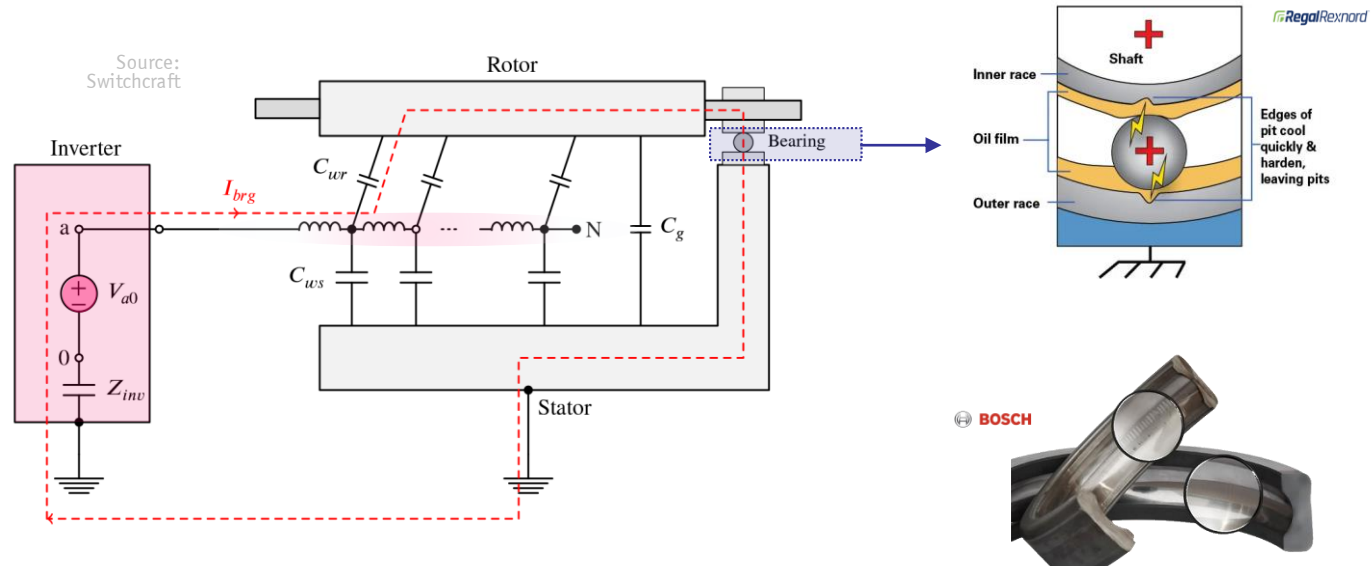
Source: YASKAWA



- *Motor Surge Voltage | CM Leakage Current | Bearing Current*

Motor Bearing Currents

- **Switching Frequency CM Inverter Output Voltage** → Motor Shaft Voltage
- **Electrical Discharge Machining ("EDM") in the Bearing**



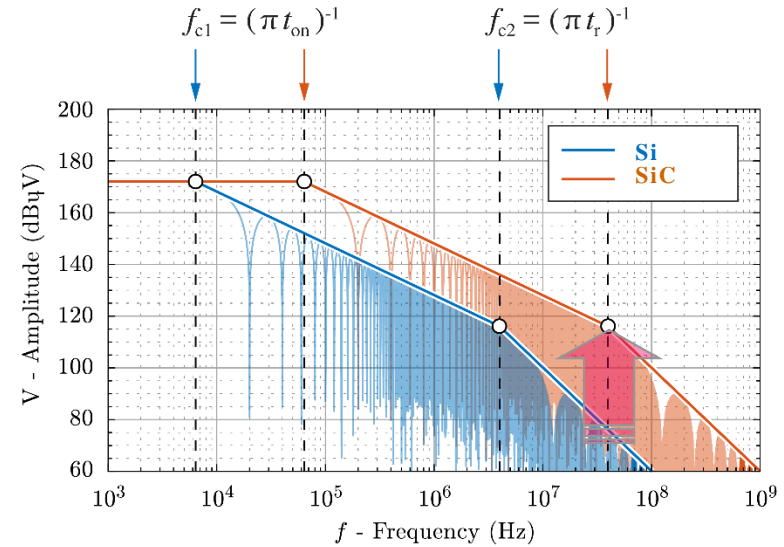
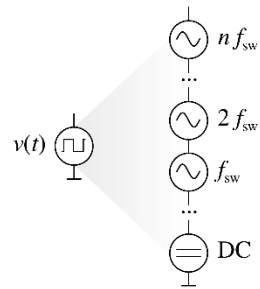
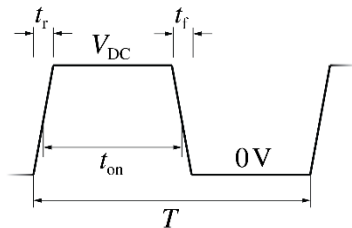
→ Cond. Grease / Ceram. Bearings / Shaft Grndg Brushes / dv/dt -Filter OR Full-Sinewave Filters

Conducted & Radiated EMI Emissions

- Higher dv/dt → Factor 10
- Higher Switching Frequencies → Factor 10
- EMI Envelope Shifted to Higher Frequencies

$f_s = 10 \text{ kHz}$ & 5 kV/us for (Si IGBT)
 $f_s = 100 \text{ kHz}$ & 50 kV/us for (SiC MOSFET)

$V_{DC} = 800 \text{ V}$
 DC/DC @ $D = 50\%$



- Higher Influence of Filter Component Parasitics & Couplings → Advanced Design

Inverter Output Filters

dv/dt-Filters
Full-Sinewave Filters

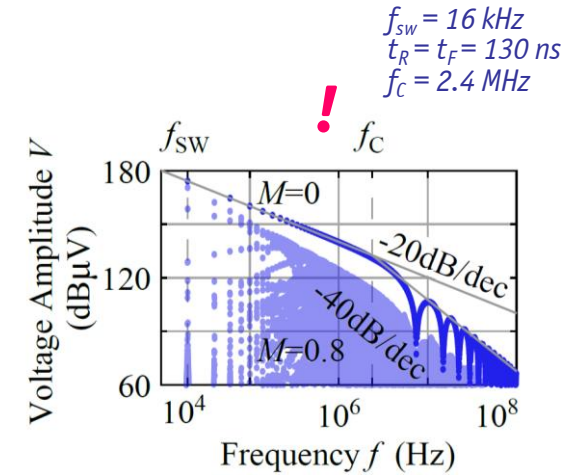
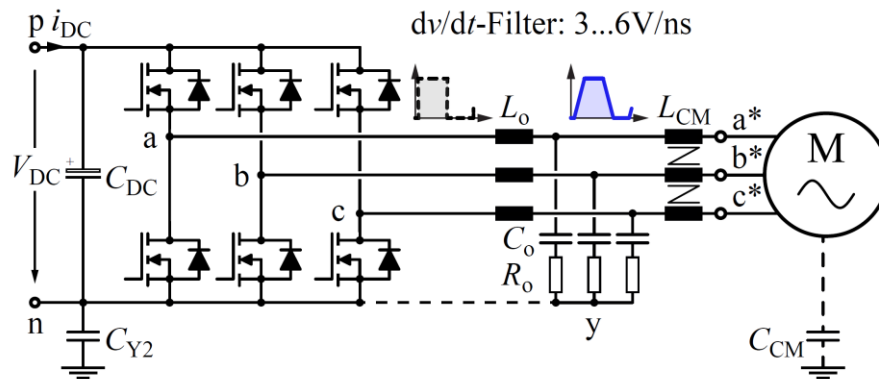




—— *dv/dt-Limitation* ——

Passive | Hybrid | Active dv/dt-Limitation

- **Passive** - Damped LC-Filter $f_c > f_s$
- **Hybrid** - Undamped LC-Filter & Multi-Step Sw. Transition
- **Active** - Gate-Drive Based Shaping of Sw. Transients

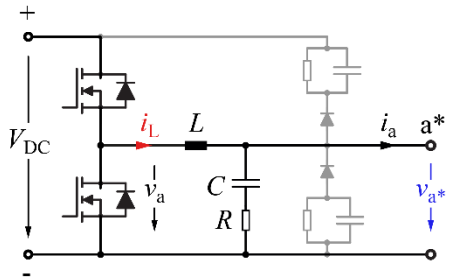


- **Connection to DC-Minus & CM Inductor** → Limit CM Curr. Spikes / EMI / Bearing Currents

Comparison of dv/dt-Filtering Techniques

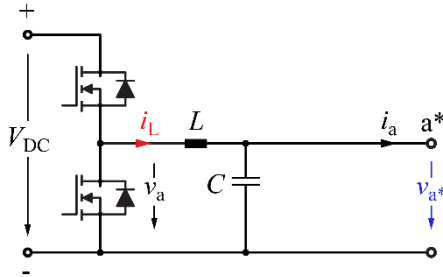
Passive Concept

1. LCR-Filter
2. Clamped LC-Filter



Hybrid Concept ($3f_{sw}$)

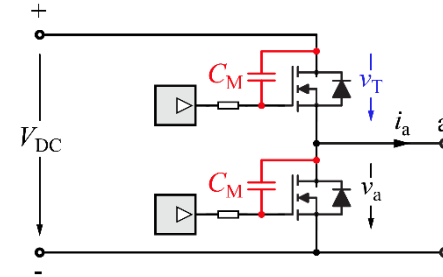
1. LC-Filter
2. Multi-Step Switching



Active Concept

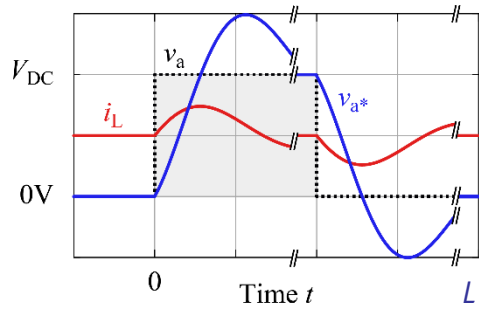


1. Miller Capacitor
2. Gate Current Control

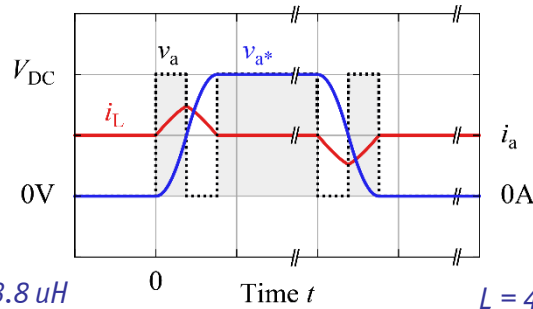


Output Voltage Waveforms — $V_{DC} = 800V, P_{out} = 10kW, 6kV/us$

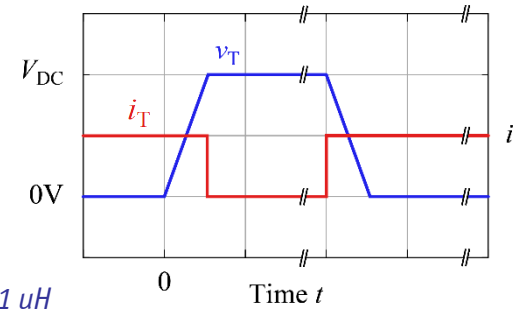
1200V SiC / 16 mΩ
 $C_M = 120 pF$



$L = 3.8 \mu H$
 $C = 2.7 nF$
 $R = 19 \Omega$

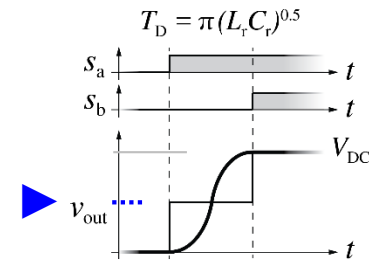
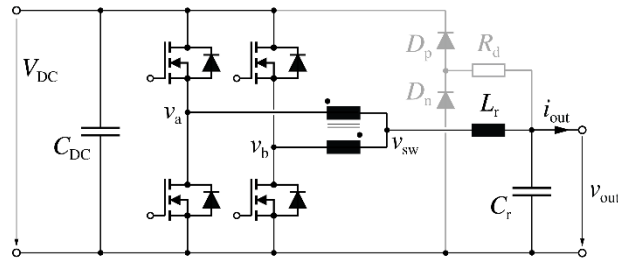


$L = 4.1 \mu H$
 $C = 1.3 nF$



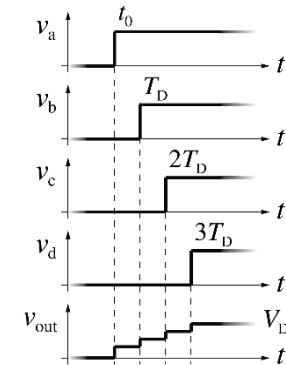
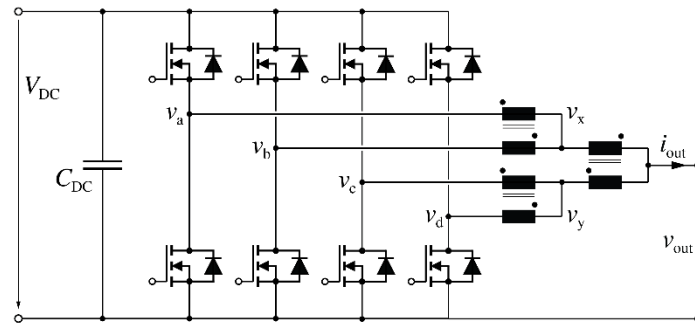
Multi-Bridge-Leg dv/dt -Limitation

■ 2-Step Switching / Resonant Transition (Hybrid dv/dt -Filter)



Source: J. Ertl et al. PCIM Europe 2018

■ Staggered Sw. Parallel Bridge-Legs → Non-Resonant Multi-Step Transition



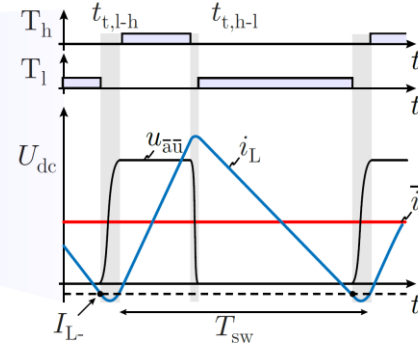
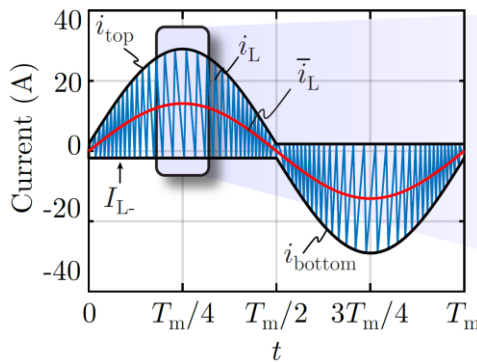
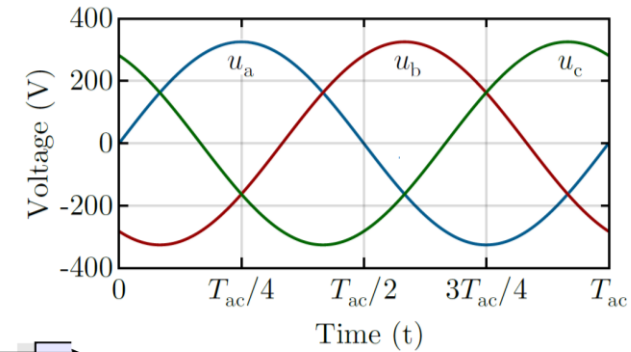
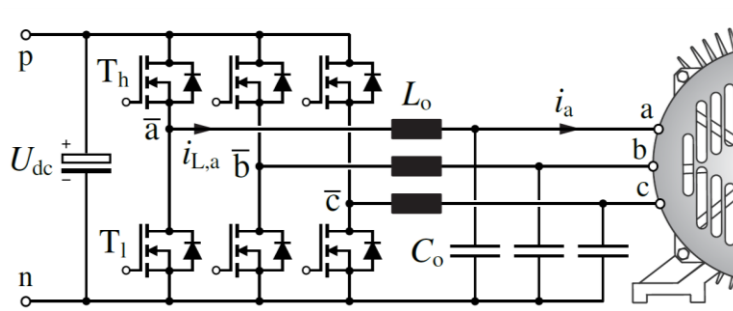
Source: J. Ertl et al. PCIM Europe 2017

- Adv. for High Power / High Output Curr. Syst. Employing Parallel Bridge-Legs & Local Comm. Caps

———— *Triangular Current Mode (TCM)* ————
ZVS Operation

Full-Sinewave Filter & ZVS Operation

- **Purely Sinusoidal Output Voltage (DM & CM Filtering)**
- **High Sw. Frequency & TCM → Low Filter Inductor Volume**
- **ZVS of Inverter Bridge-Legs**

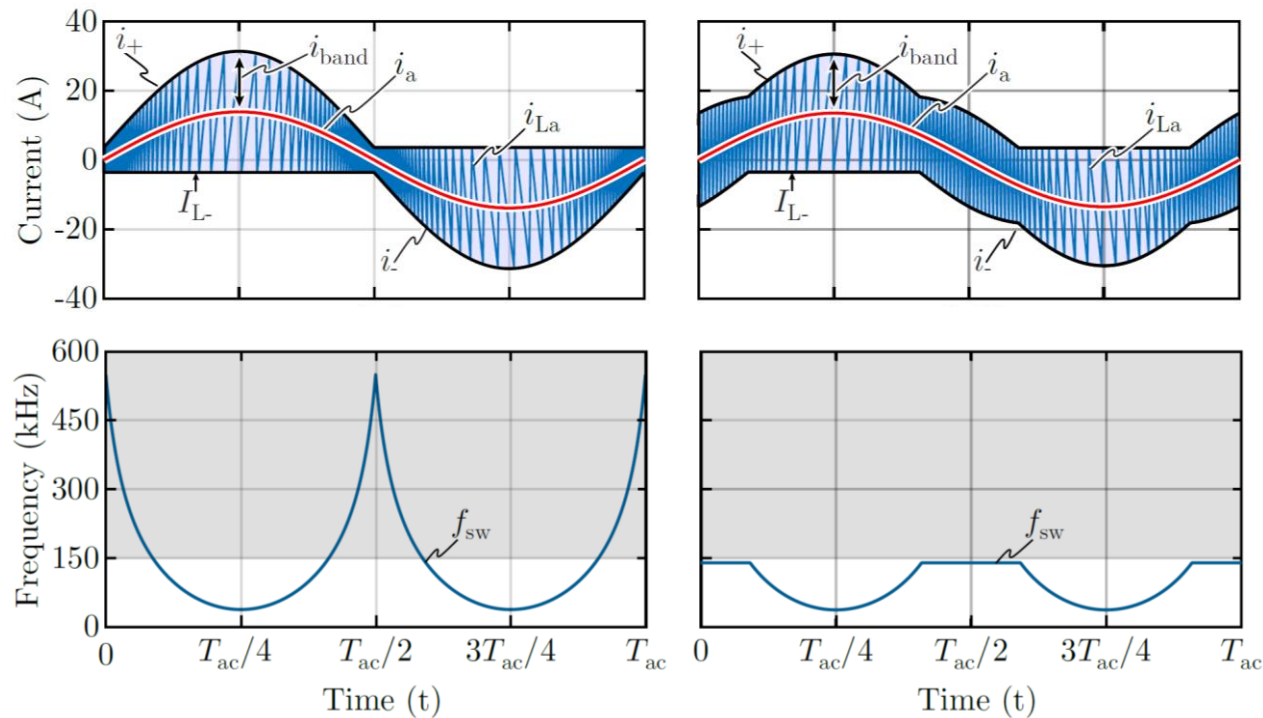


NFO Sinus

- **Only 33% Increase of Transistor Conduction Losses Compared to CCM (!)**
- **Very Wide Switching Frequency Variation**

Frequency-Bounded TCM → B-TCM

- Very Wide Switching Frequency Variation of TCM → B-TCM



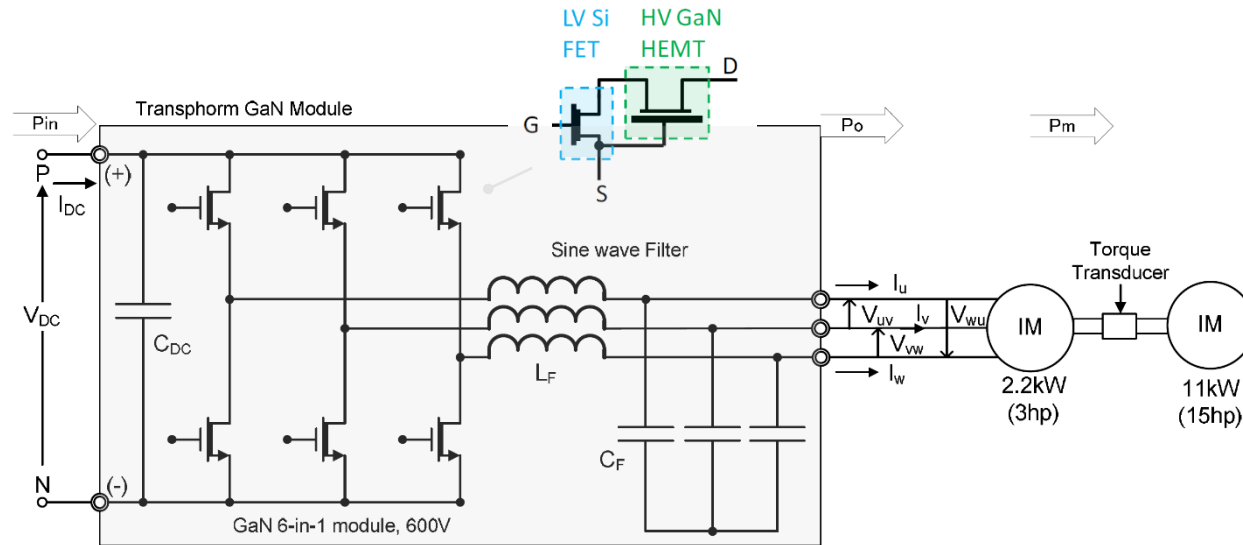
- TCM → B-TCM — 10% Further Increase of Transistor Conduction Losses

—— *Continuous Current Mode (CCM) Operation* ——

3-Φ 650V GaN Inverter System (1)

Source: YASKAWA

- **Transphorm 650V Normally-On GaN HEMT/30V Si-MOSFET Cascode 6-in-1 Power Module**
- **Sinewave LC Output Filter** — Corner Frequency $f_c = 34\text{ kHz}$ ($f_{sw} = 100\text{ kHz}$)
- **No Freewheeling Diodes**

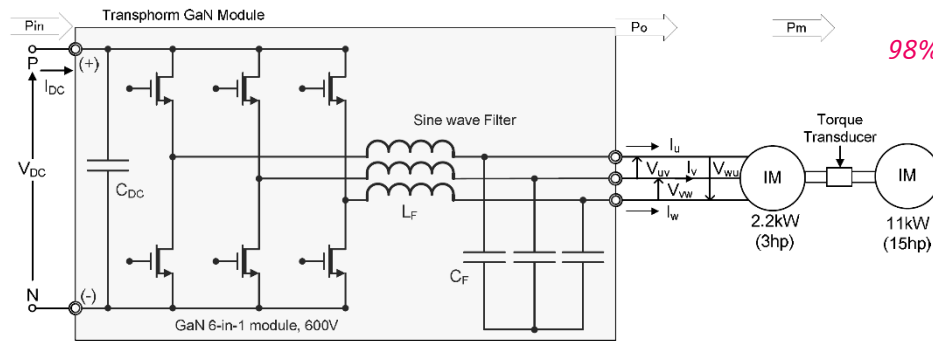


→ Comparison to Si-IGBT Drive Systems

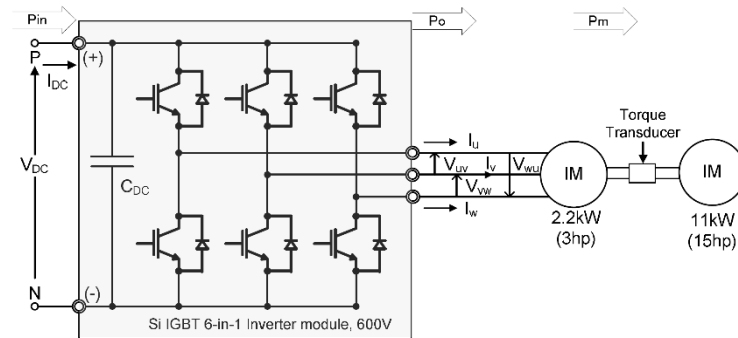
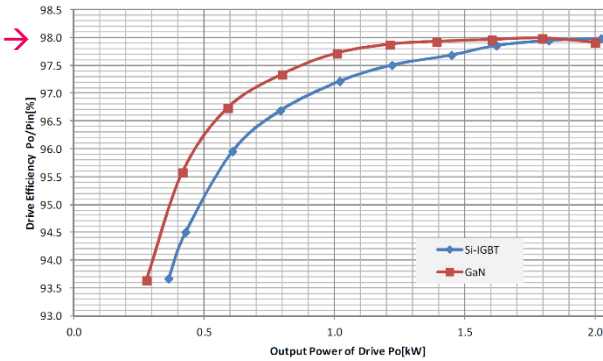
3- Φ 650V GaN Inverter System (2)

Source: YASKAWA

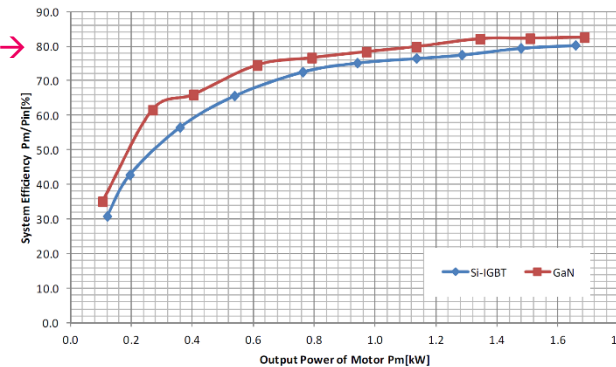
- Comparison of **GaN Inverter w/ LC-Filter** to **Si-IGBT System (No Filter, $f_{sw}=15$ kHz)**
- **Measurement of Inverter Stage & Overall Drive Losses @ 60 Hz**



98% →



80% →



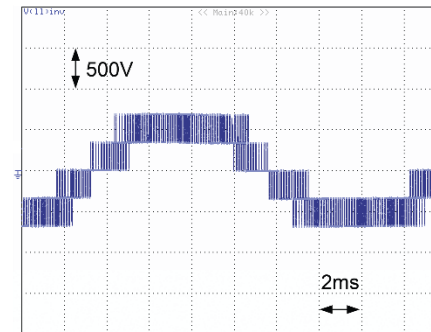
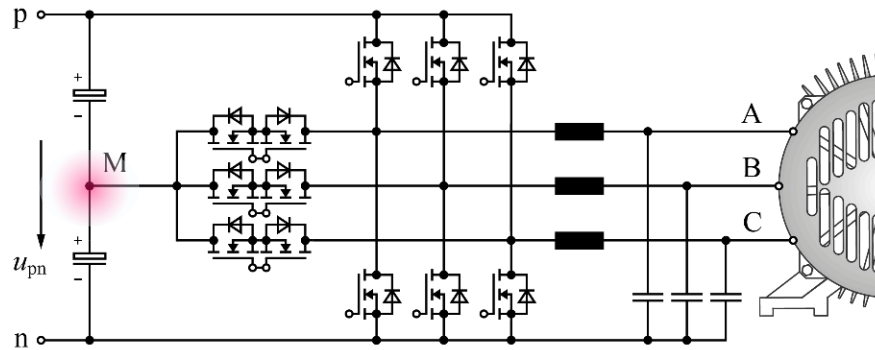
→ **2% Higher Efficiency of GaN System Despite LC-Filter (Saving in Motor Losses) !**



— *Multi-Level / Multi-Cell
Converters & Modularity* —

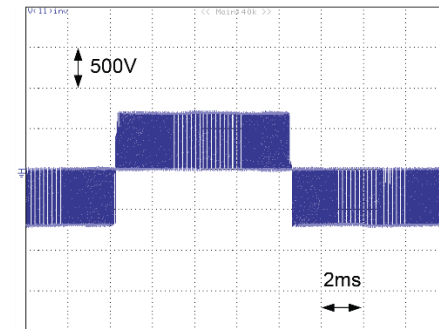
3-Level T-Type Inverter (1)

- Higher Number of Bridge-Leg Output Voltage Levels / Lower DM & CM Voltage Steps
- Neutral Point Clamped | Flying Capacitor | T-Type Bridge-Leg Topologies



3-Level Bridge-Leg

Motor Line-to-Line Voltage

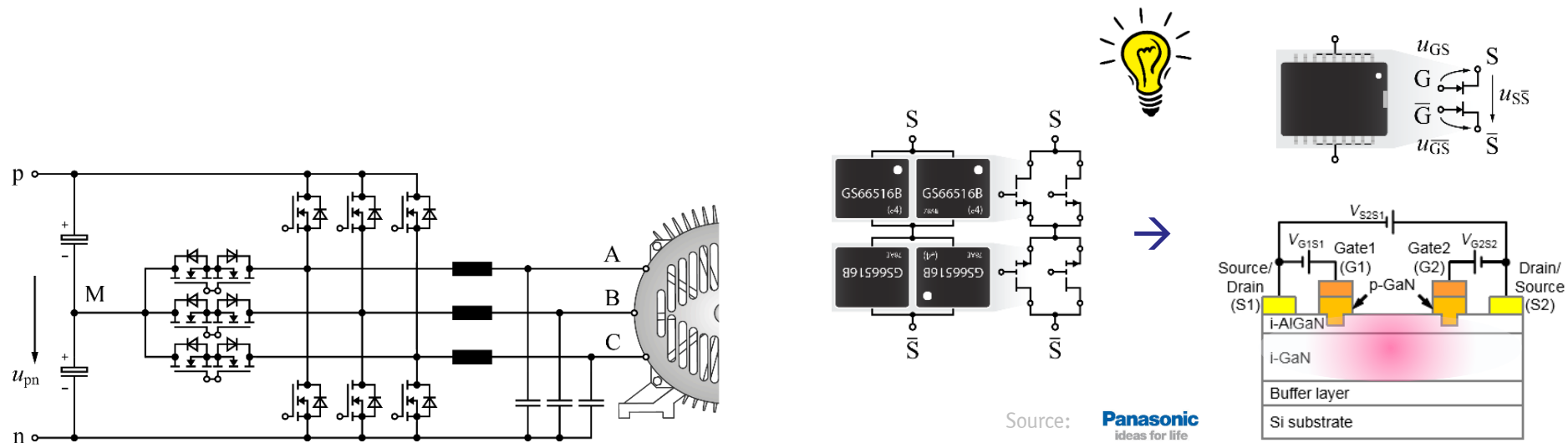


2-Level Bridge-Leg

- More Complicated Bridge-Leg Structure
- On-State-Losses of Series-Connected Switches

3-Level T-Type Inverter (2)

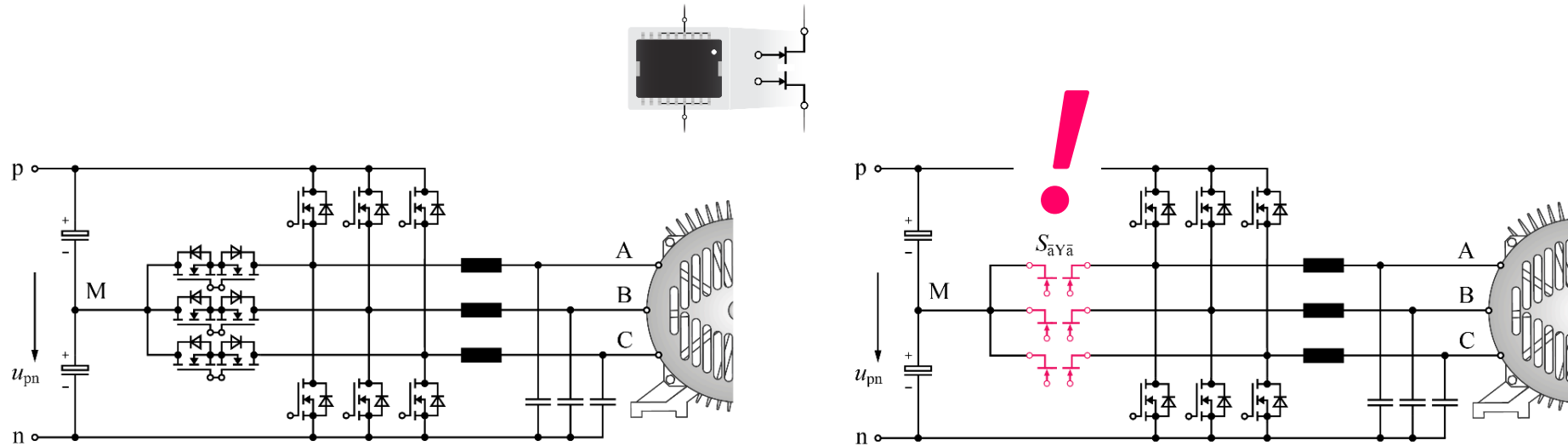
- 3-Level T-Type Inverter — 3-Level Phase Voltage / 5-Level Line-to-Line Voltage
- Lower DM & CM Voltage Steps Compared to 2-Level Converter



- Full-Sinewave DC-Link Referenced LC-Filter — Elimination of DM & CM Sw. Frequ. Voltage Harmonics
- T-Type Topology Ensures Low Conduction Losses — Adv. Application of M-BDSs (!)

3-Level T-Type Inverter (3)

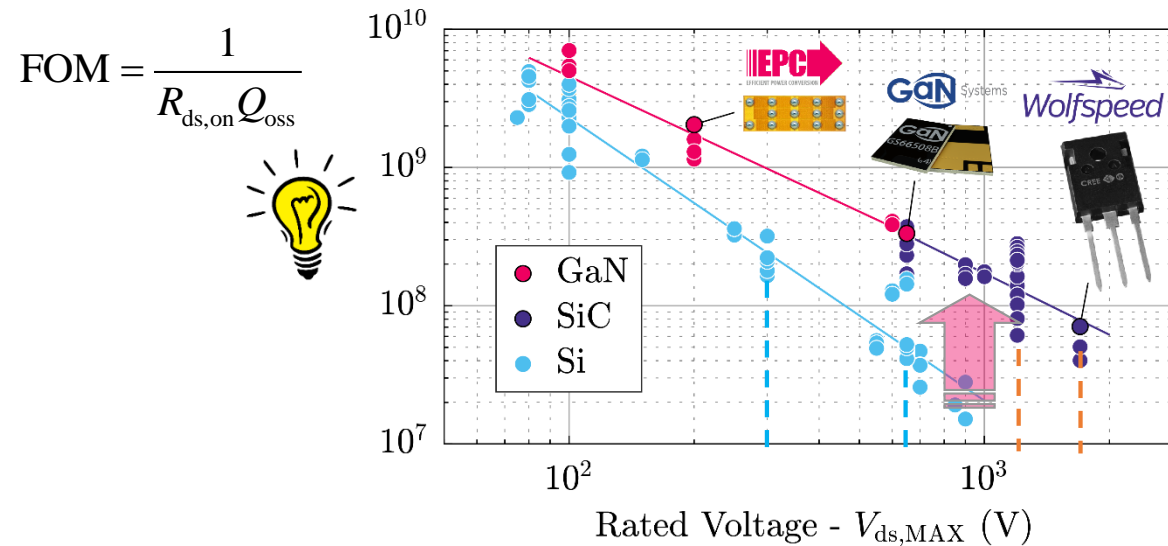
- *3-Level T-Type Inverter — 3-Level Phase Voltage / 5-Level Line-to-Line Voltage*
- *Lower DM & CM Voltage Steps Compared to 2-Level Converter*



- *Full-Sinewave DC-Link Referenced LC-Filter — Elimination of DM & CM Sw. Frequ. Voltage Harmonics*
- *T-Type Topology Ensures Low Conduction Losses — Adv. Application of M-BDSs (!)*

SiC/GaN Figure-of-Merit

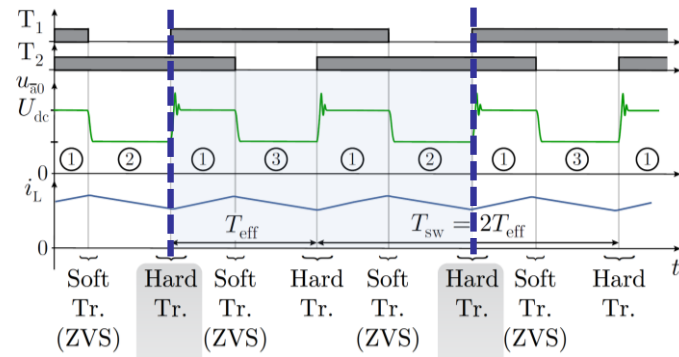
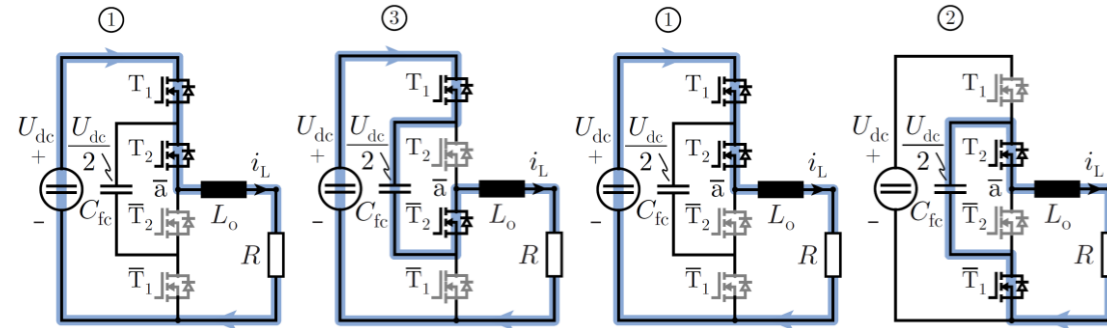
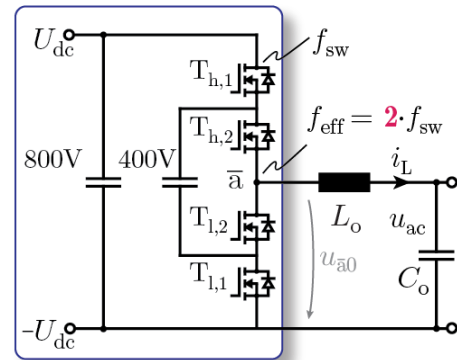
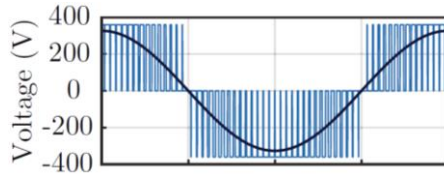
- *Figure-of-Merit (FOM) Quantifies Conduction & Switching Properties*
- *FOM Identifies Max. Achievable Efficiency @ Given Sw. Frequ.*



- *Advantage of LV over HV Power Semiconductors →*
- *Advantage of Multi-Level over 2-Level Converter Topologies*

3-Level Flying Capacitor (FC) Converter

- 3-Level Flying Cap. (FC) Converter → No Connection to DC-Midpoint
- Involves All Switches in Voltage Generation → Eff. Doubles Device Sw. Frequency

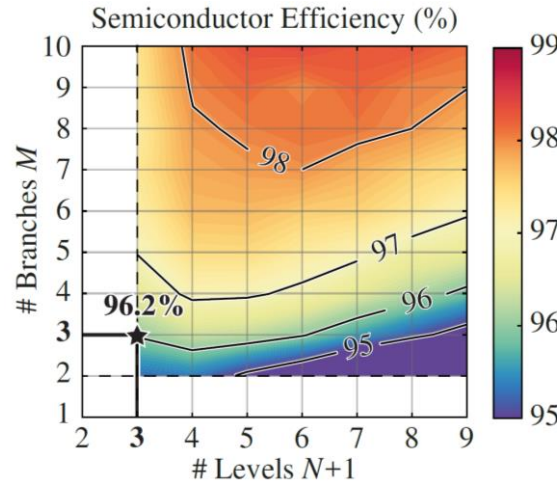
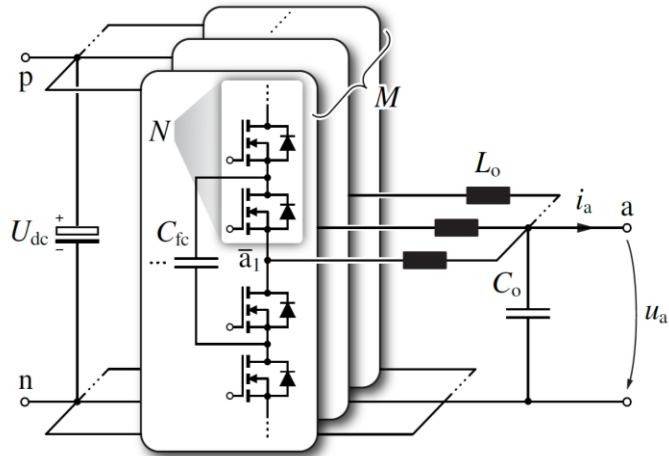


- FC Voltage Balancing Possible also for DC Output (!)

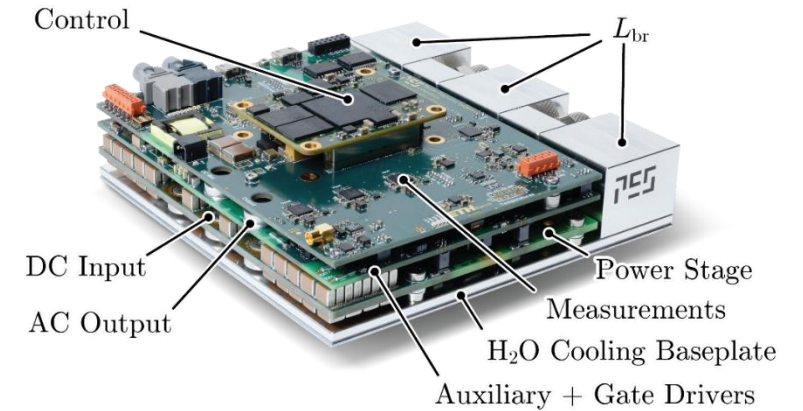
4.8MHz GaN Half-Bridge Phase Module

■ Combination of *Series & Parallel Interleaving*

- 600V GaN Power Semiconductors, $f_{sw} = 800\text{ kHz}$
- Volume of $\approx 180\text{ cm}^3$ (incl. Control etc.)
- H_2O Cooling Through Baseplate



 25 kW/dm^3



- Operation @ $f_{out} = 100\text{ kHz} / f_{sw,eff} = 4.8\text{ MHz}$, 10 kW , $U_{dc} = 800\text{ V}$

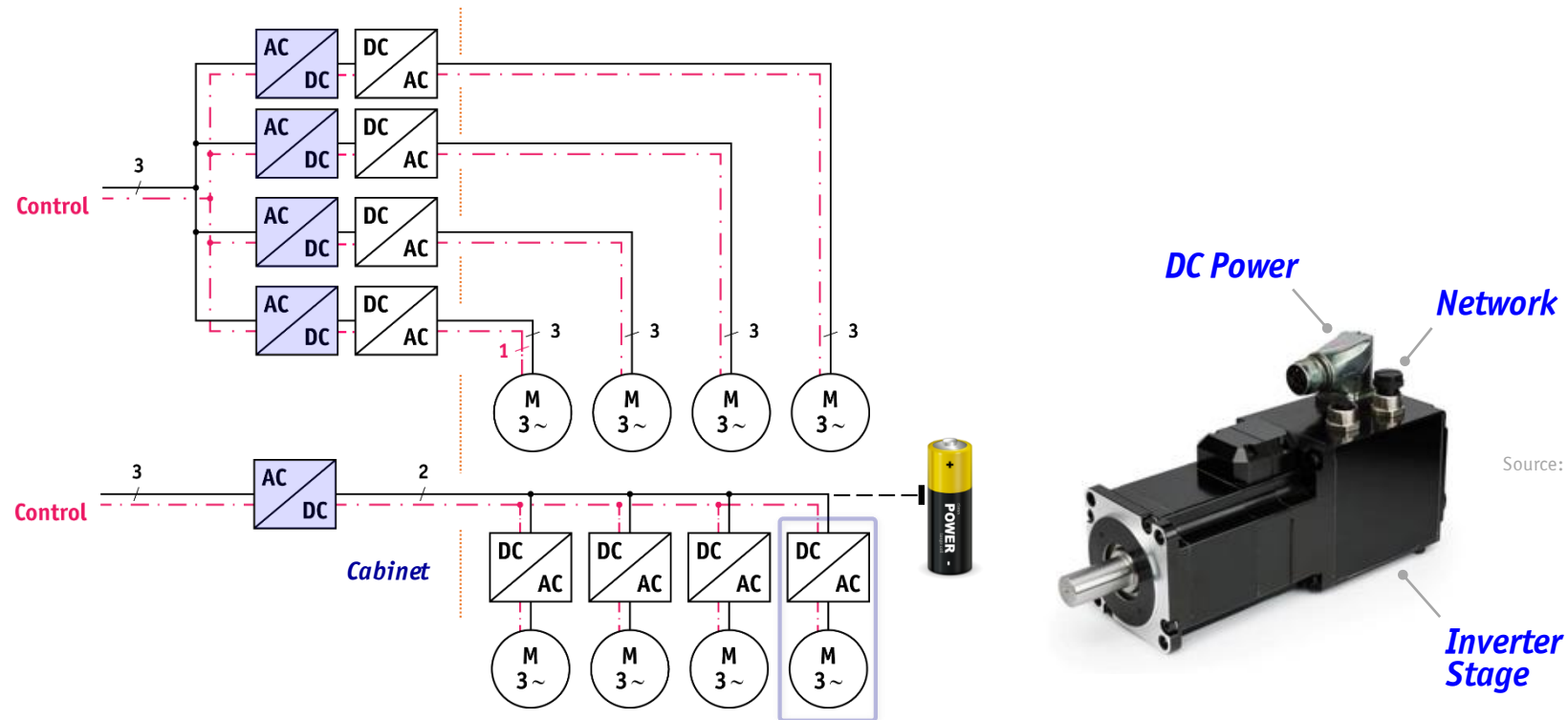


———— *Motor-Integrated
Inverter Systems* ————



Multi-Axis Drive Systems

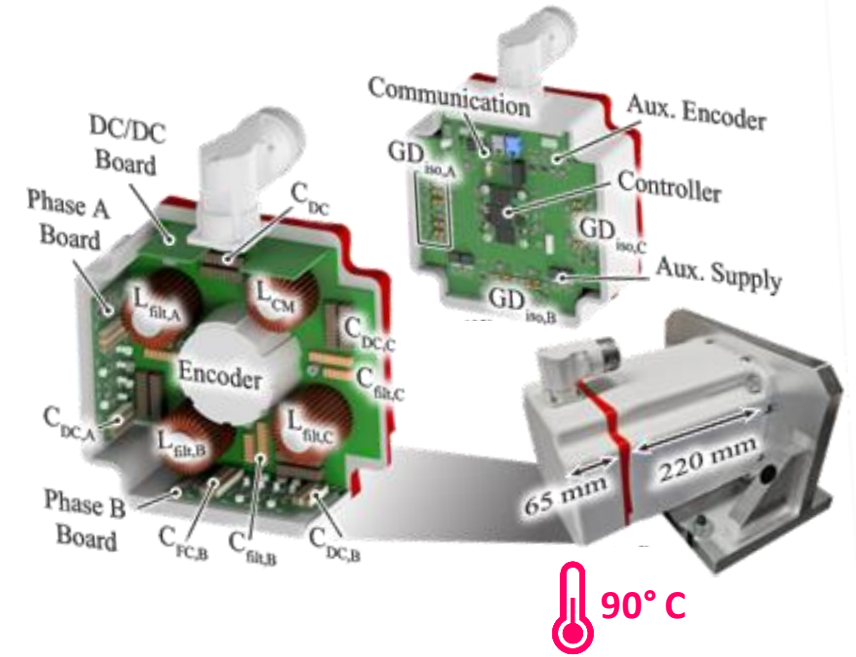
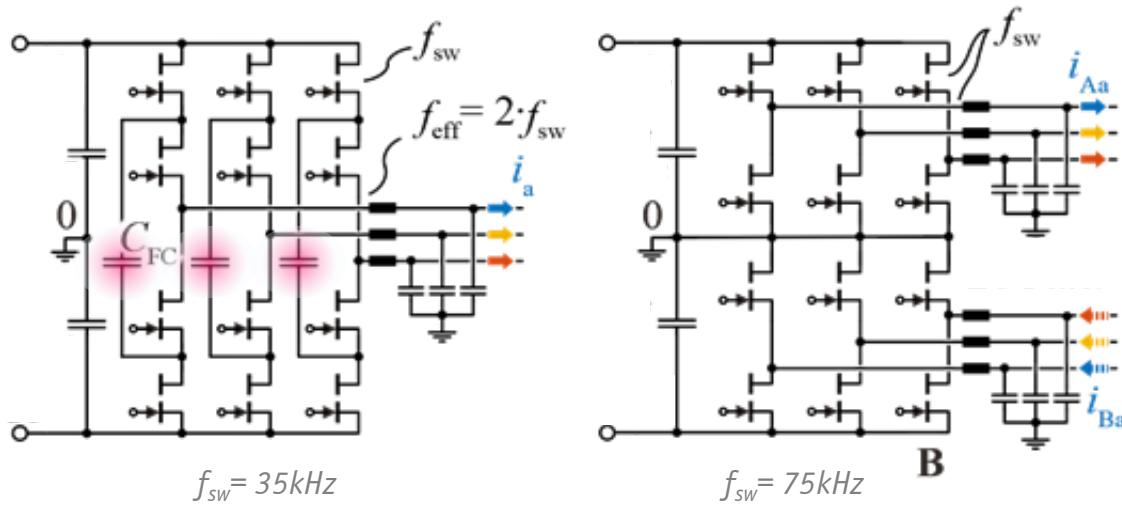
- **Common DC-Bus** — **Single AC/DC Converter / Smaller Cabinet**
- **Motor Integration of DC/AC Stage** — **Massive Saving in Cabling Effort / Simplified Installation**



- **Facilitates DC-Bus Energy Buffer**
- **Direct Energy Exchange @ DC-Bus / Higher Efficiency / Unidir. Front-End**

Motor Integrated Inverter Stage

- **Comparative Evaluation of ML-Inverter Concepts**
- **2x 2-Level Stacked 650V GaN | 3-Level 650V GaN | 7-Level 200V Si Inverter**
- **Design for 800V DC-Link / 7.5kW / 99% Efficiency / 3s 3x T_N Overload**



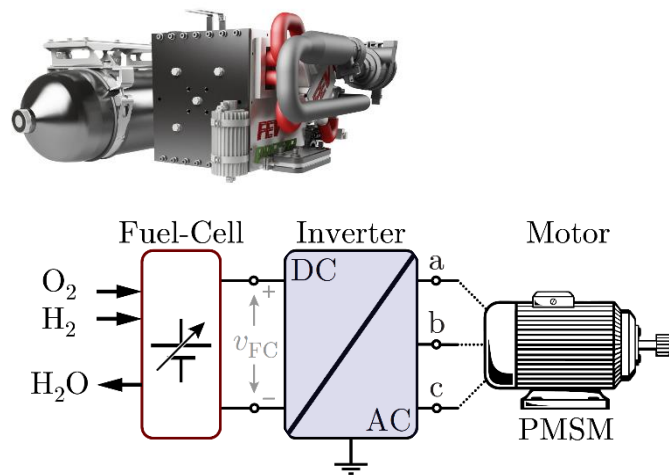
- **7-Level FC Inverter** — Large PCB Area Requirement & High Complexity
- **2x 2-Level Inverter** — No Flying Capacitors & CM Cancellation / Low L_{CM} Volume
- **3-Level FC Inverter** — Best Overall Trade-Off (Complexity / PCB Area / Volume of Full-Sinewave Filter etc.)

*Buck-Boost
Functionality* 

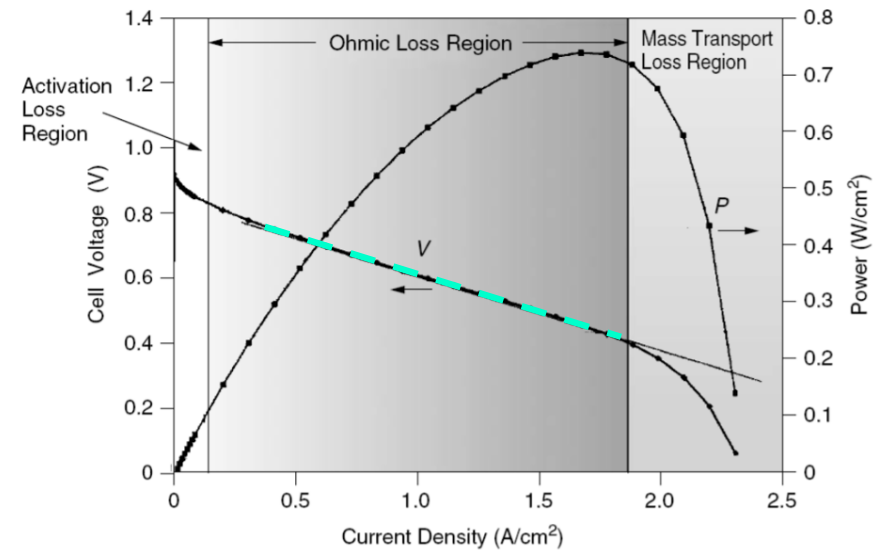
Motivation

- **General / Wide Applicability**
 - **Adaption to Load-Dependent Battery | Fuel Cell Supply Voltage**
 - **Operation in Wide Output Voltage / Wide Motor Speed Range**

Source: magazine.fev.com



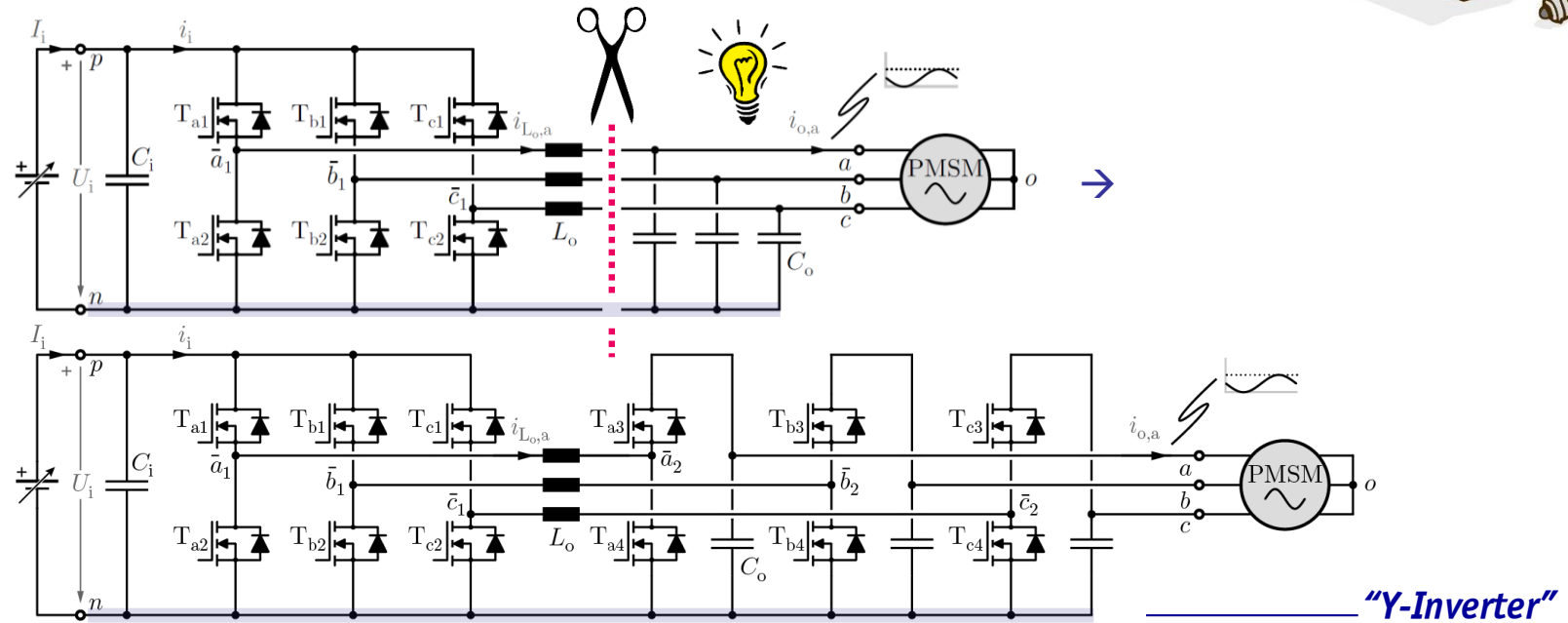
Source: www.chegg.com



- **Full-Sinewave Filtered Motor Supply Voltage**
- **LC Output Filter Inductor Advantageously Utilized as Buck-Boost-Inductor**

Buck-Boost «Y-Inverter»

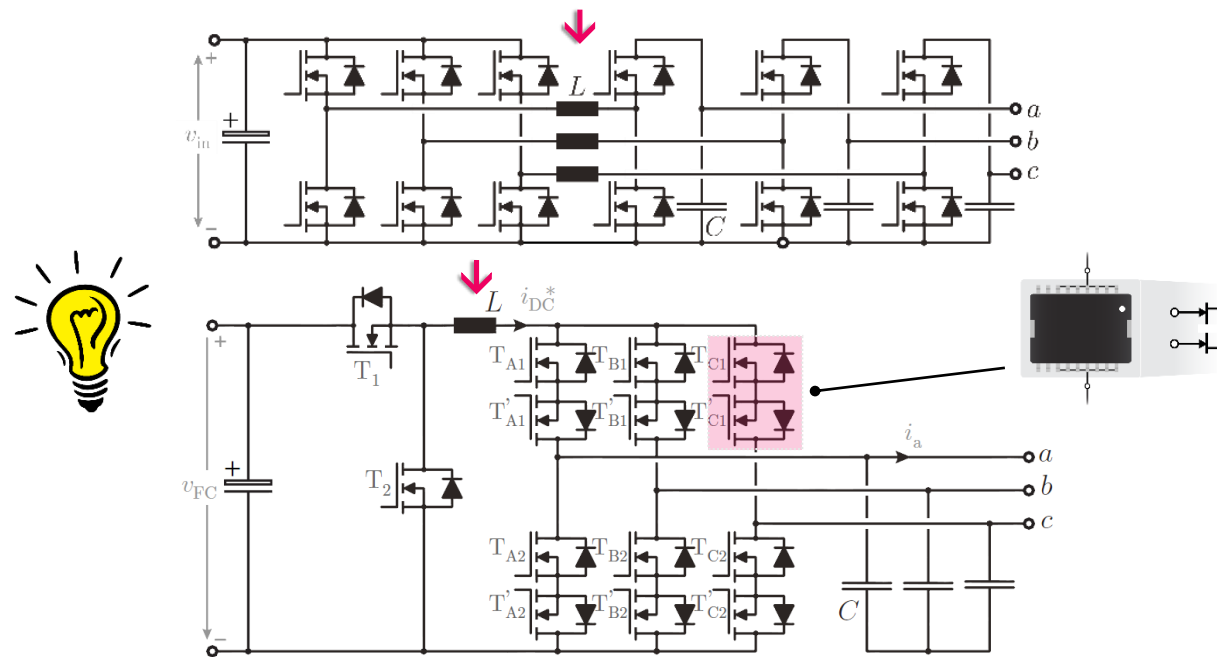
- Generation of AC-Voltages Using Unipolar Bridge-Legs



- Switch-Mode Operation of **Buck OR Boost Stage** → **Quasi Single-Stage Energy Conversion (!)**
- **3-Φ Continuous Sinusoidal Output / Low EMI** → **No Shielded Cables / No Motor Insul. Stress**

3- Φ Current Source Inverter (CSI) Topology

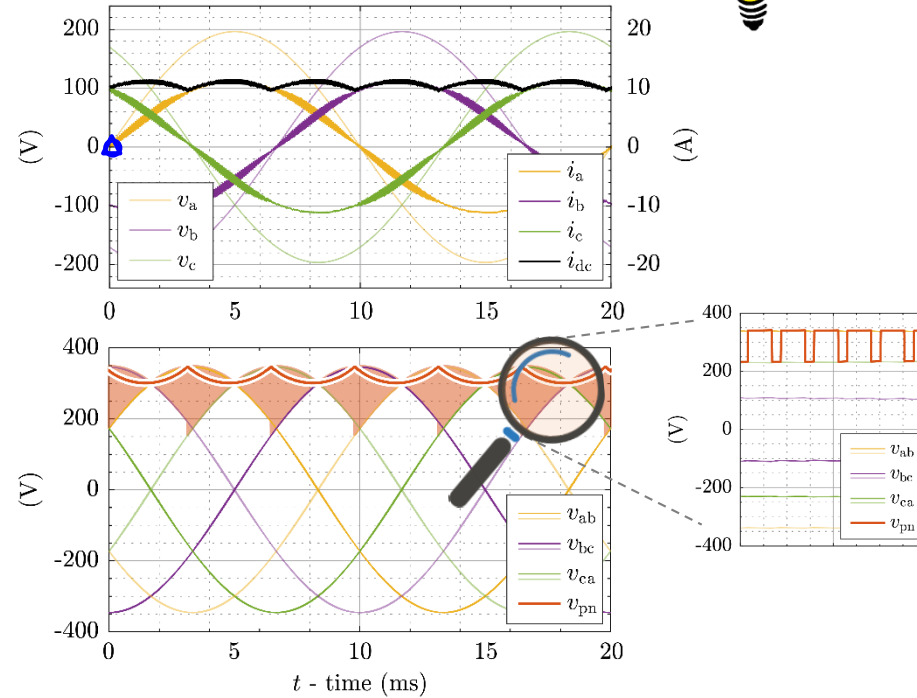
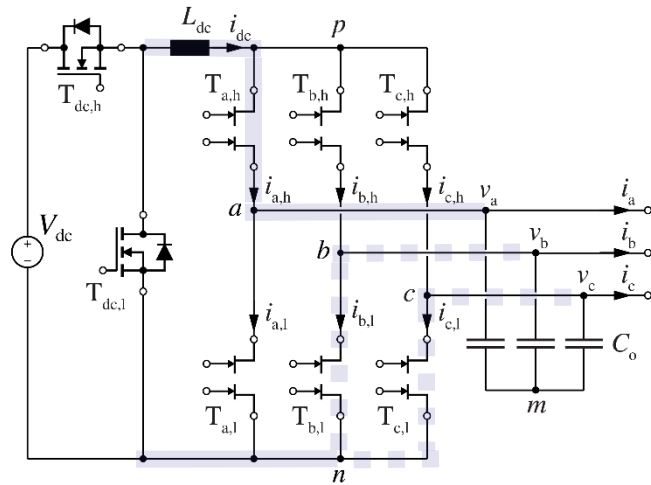
- **Y-Inverter** \rightarrow Phase Modules w/ Buck-Stage | Current Link | Boost-Stage
- **3- Φ CSI** \rightarrow Buck-Stage $V \rightarrow I$ Converter | Current DC-Link DC/AC-Stage



- **Single Inductive Component**
- **Positive DC-Side Voltage for Both Directions of Power Flow** \rightarrow Future Utilization of M-BDSs

3-Φ Buck-Boost CSI Modulation

- **“Synergetic” Control of Buck-Stage & CSI Stage**
- **6-Pulse-Shaping of DC Current by Buck-Stage** → **Allows Clamping of One CSI-Phase**



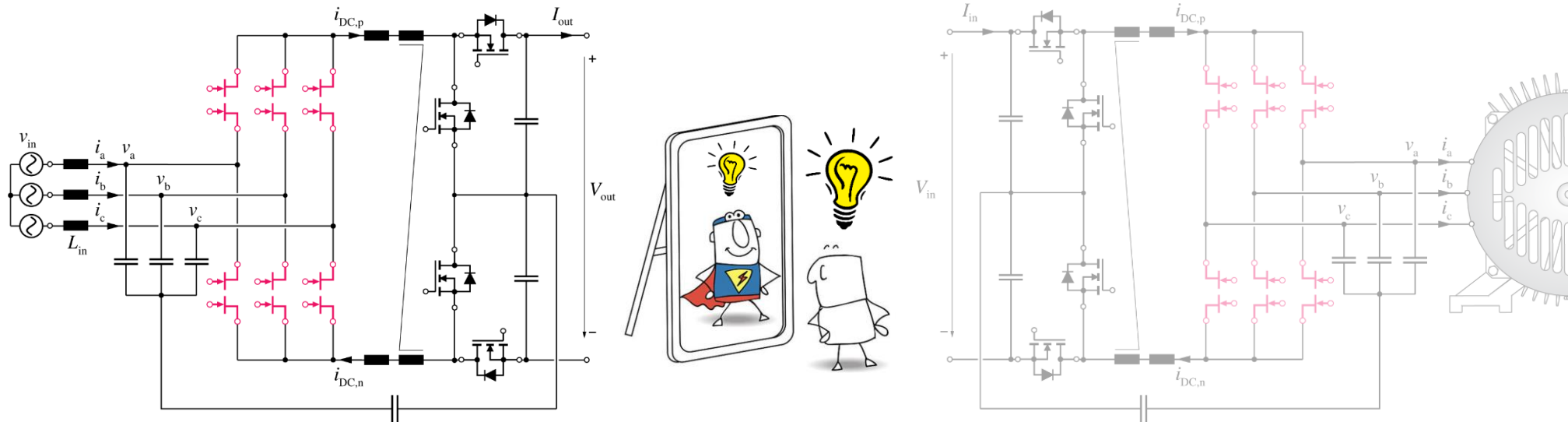
- **Switching of Only 2 of 3 Phase Legs (2/3 Mode)** → **Significant Reduction of Sw. Losses**

3- Φ AC/AC Conversion



Derivation of 3- Φ Current Source AC/AC Converter (1)

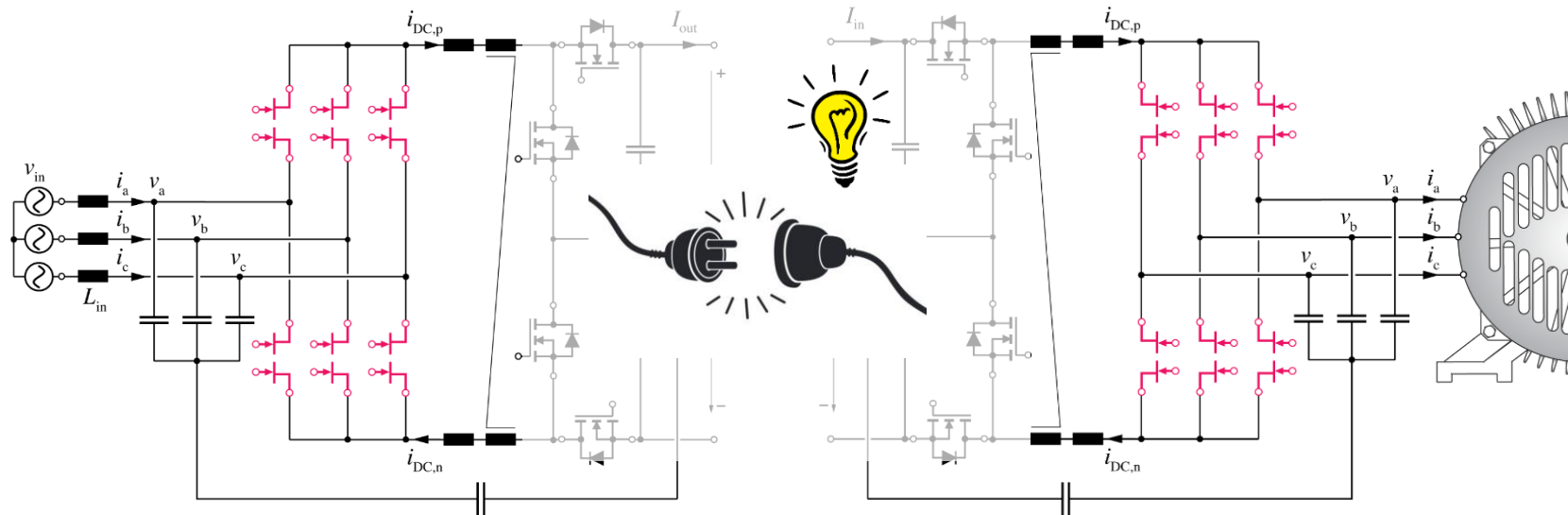
- **Derivation Based on Bidir. Buck-Boost Current Source Inverter (CSI) \rightarrow Buck-Boost PFC Rectifier (CSR)**
- **Lower # of Ind. Components Compared to Boost-Buck Rectifier Approach**



- **AC/DC Buck Stage Distributes DC-Link Current to Mains Phases — Sinusoidal Inp. Current**
- **Synergetic Control/Modulation of Rectifier Stage & DC/DC Stage for Min. Sw. Losses**

Derivation of 3- Φ Current Source AC/AC Converter (2)

- *DC-Side Coupling of Buck-Boost Current DC-Link PFC Rectifier & Inverter — AC/DC/AC*
- *Full-Sinewave Filtering @ Input & Output w/ Single Magnetic Component*

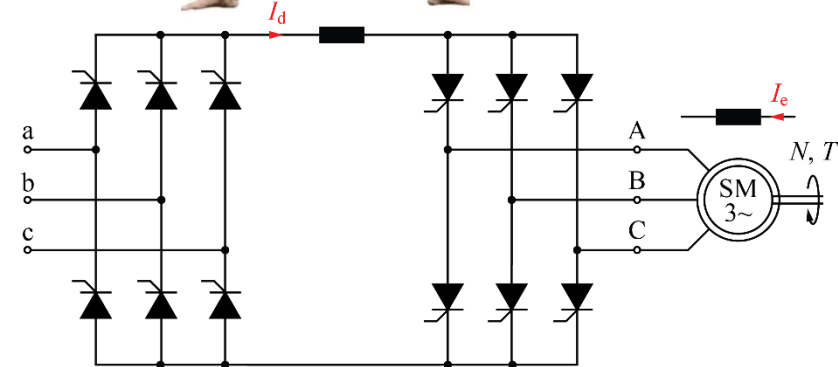
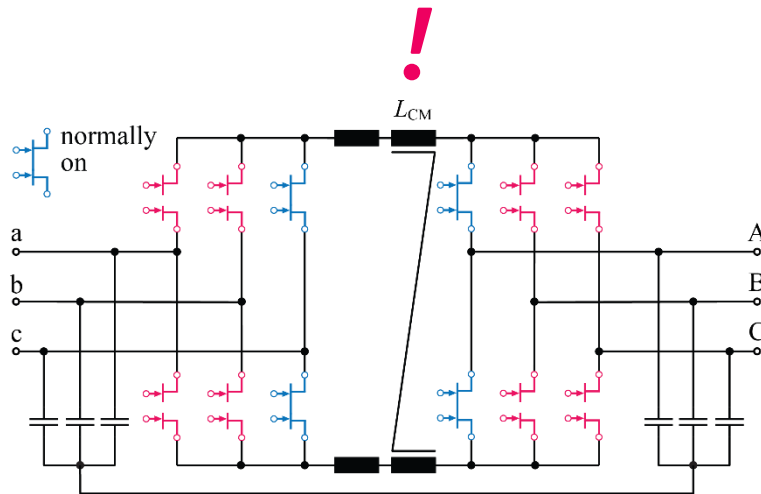


- *Bipolar Blocking / Unidir. Switches | Unidir. DC-Link Current Sufficient for Bidir. Power Conversion*
- *Modulation-Based Inversion of DC-Link Voltage Polarity → Inv. of Power Flow Direction*

3- Φ Current Source AC/AC Converter

- **Sinusoidal Motor Voltage Achieved w/ Single Ind. Component**
- **Unidir. Valves Sufficient for Bidir. Power Conversion**
- **M-BDSs — Synchronous Rectification**

Source: www.mb-drive-services.com



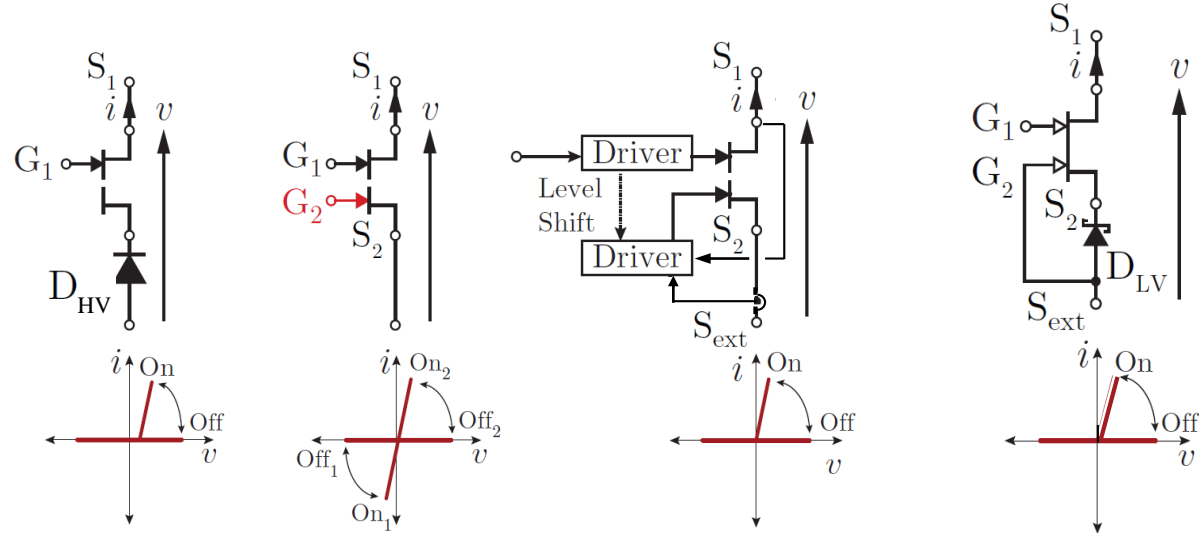
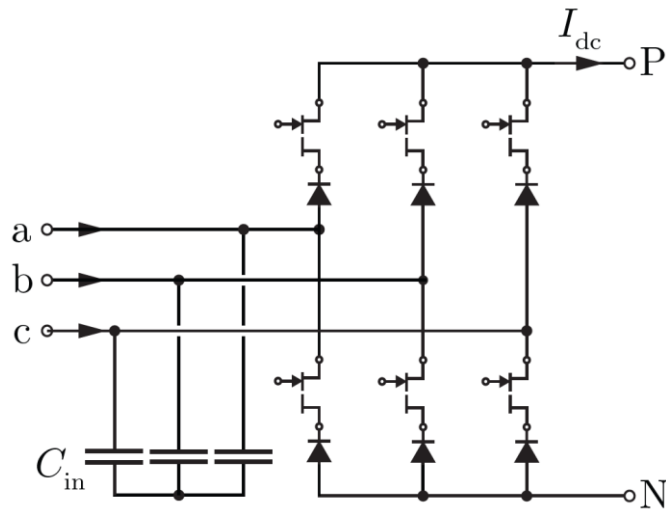
- **Relation to High-Power Thyristor-Based Medium-Voltage Synchr. Machine Variable Speed Drives**

Remark Self Reverse-Blocking M-BDS-Concept (1)

■ Bidir. Curr. DC-Link Converters — Unidir. I_{dc} & Bipolar U_{dc} OR Bidir. I_{dc} & Unipolar U_{dc}

- HV Switch + HV Diode
- M-BDS
- "Self-Switching"

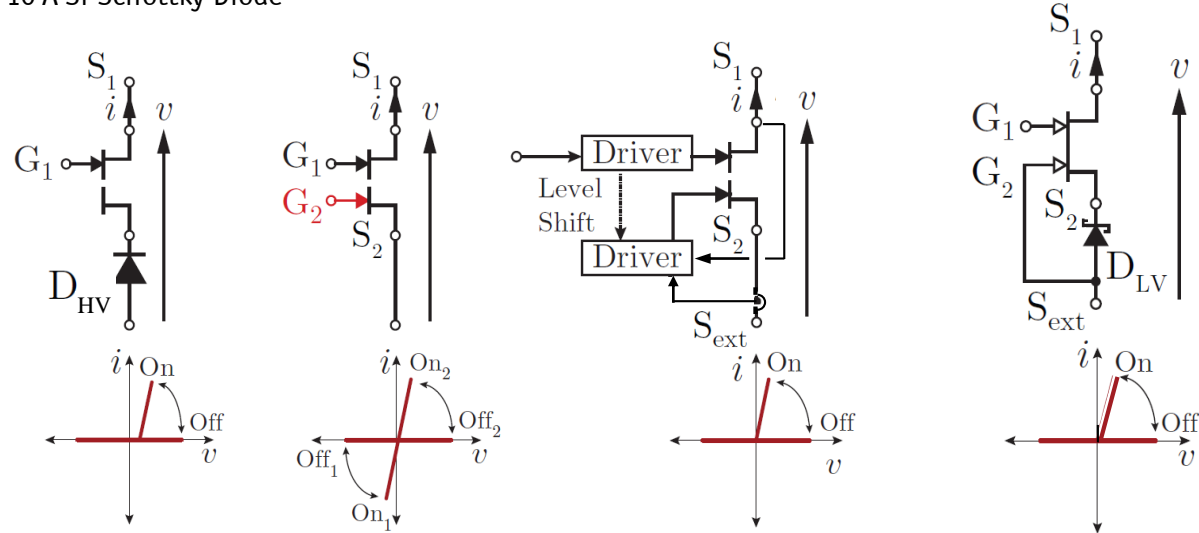
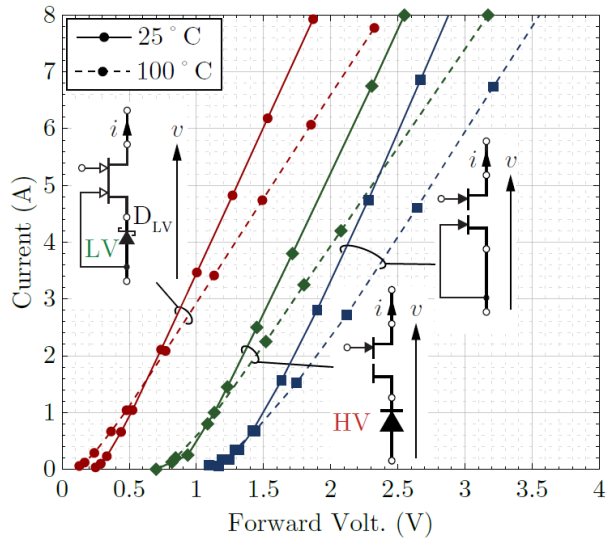
HV Diode Characteristic / High Cond. Losses
 Ohmic Cond. Char. BUT 2 External Gate Signals / 2 Gate Drivers
 Ohmic Cond. Char. BUT High Local Complexity (Sensing)



• SRB-MBDS Quasi-Ohmic Cond. Char. (Cascode w/ LV Si Schottky Diode) & 1 External Gate

Remark Self Reverse-Blocking M-BDS-Concept (2)

- **Bidir. Curr. DC-Link Converters** — **Unidir. I_{dc} & Bipolar U_{dc}** OR **Bidir. I_{dc} & Unipolar U_{dc}**
 - **HV Switch + HV Diode** **HV Diode Characteristic / High Cond. Losses**
 - **M-BDS** **Ohmic Cond. Char. BUT 2 External Gate Signals / 2 Gate Drivers**
 - **“Self-Switching”** **Ohmic Cond. Char. BUT High Local Complexity (Sensing)**



- **SRB-MBDS** **Quasi-Ohmic Cond. Char. (Cascode w/ LV Si Schottky Diode) & 1 External Gate**



DUALITY

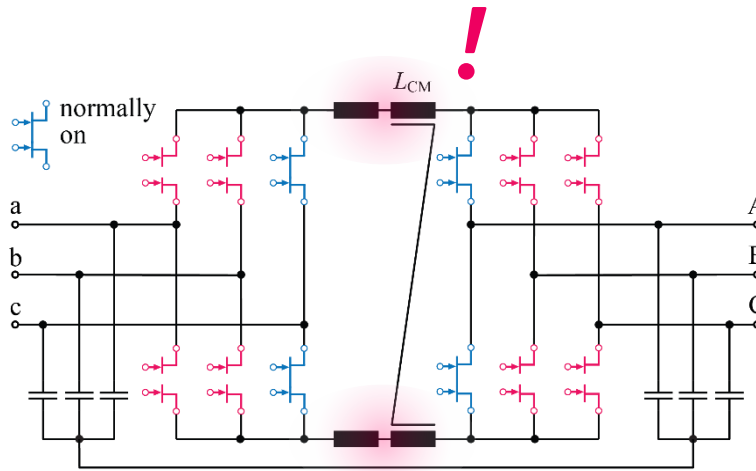
Buck-
Boost

Boost-
Buck

DUALITY

■ Current DC-Link Topology

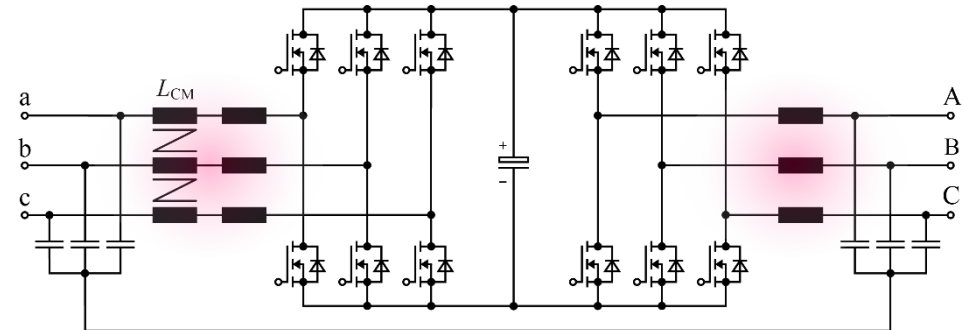
- Application of *M-BDSs*
- Complex 4-Step Commutation OR *SRB-MBDSs*
- *Low Filter Volume*



- Challenging *Overvoltage Protection*
- *Limited Control Dynamics*

■ Voltage DC-Link Topology

- *Standard Bridge-Legs*
- *Low-Complexity Commutation*
- *Defined Semiconductor Voltage Stress*
- *Facilitates DC-Link Energy Storage*

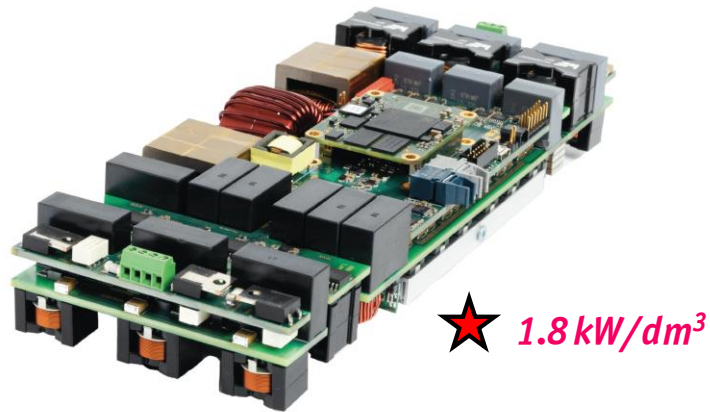


- *High Input / Output Filter Volume*

DUALITY

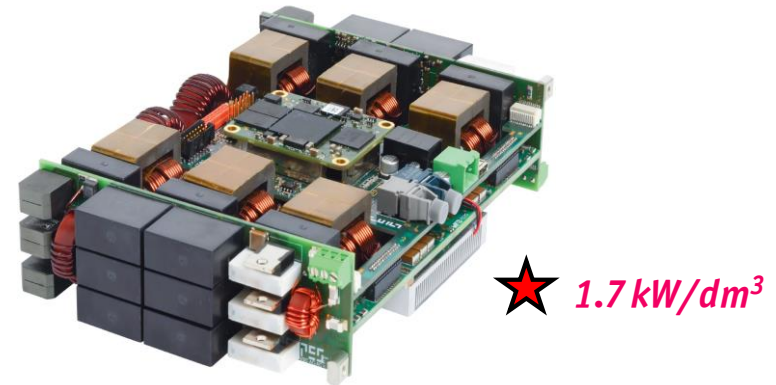
■ *Current DC-Link Topology*

- *Application of M-BDSs*
- *Complex 4-Step Commutation*
- *Low Filter Volume*



■ *Voltage DC-Link Topology*

- *Standard Bridge-Legs*
- *Low-Complexity Commutation*
- *Defined Semiconductor Voltage Stress*
- *Facilitates DC-Link Energy Storage*



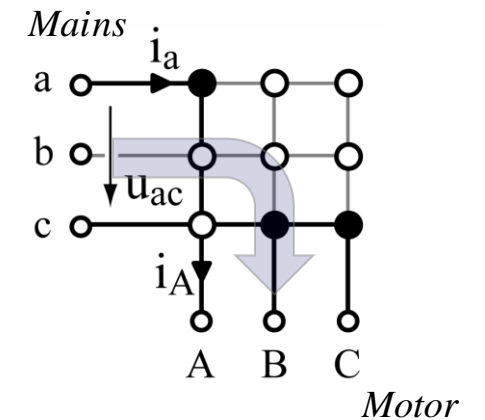
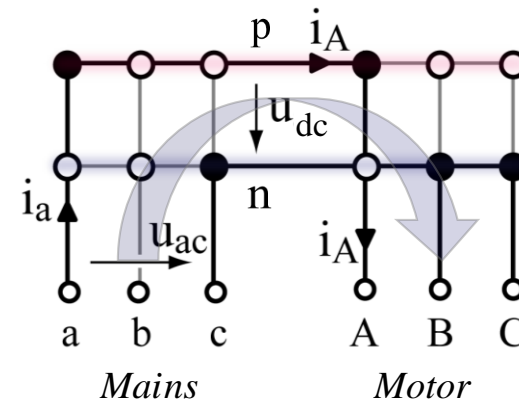
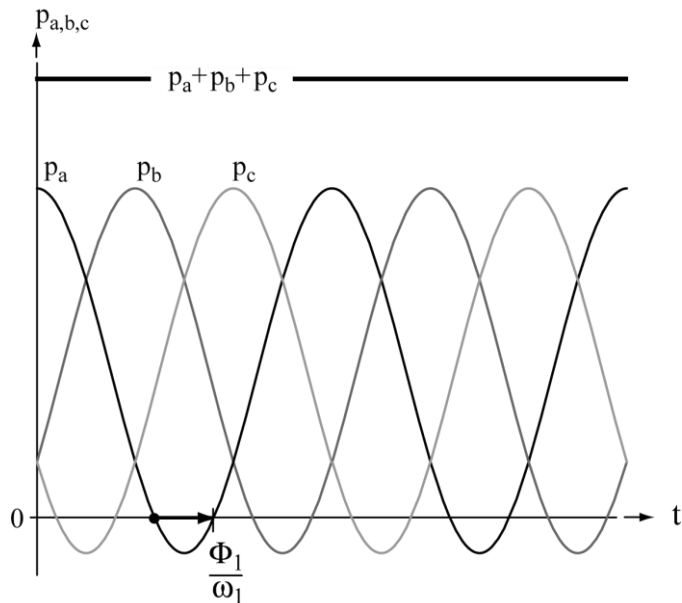
- *All-600 V-GaN AC-AC VSDs / 1.4 kW, 200 V L-L / Full EMI Filter (Grid & Motor) / 97% Nominal Eff.*

3- Φ AC/AC Matrix Converter

$$\begin{Bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 1 & 1 \end{Bmatrix}$$

Indirect & Direct 3- Φ AC/AC Matrix Converter

- **Constant 3- Φ Instantaneous Power Flow \rightarrow No Low-Freq. DC-Link Power Pulsation Buffer Requirement (!)**
- **Indirect AC/DC—DC/AC OR Direct AC/AC Power Conversion \rightarrow IMC OR DMC**
- **DMC \rightarrow Switch Matrix w/ Bipolar Voltage Blocking & Current Carrying Devices**

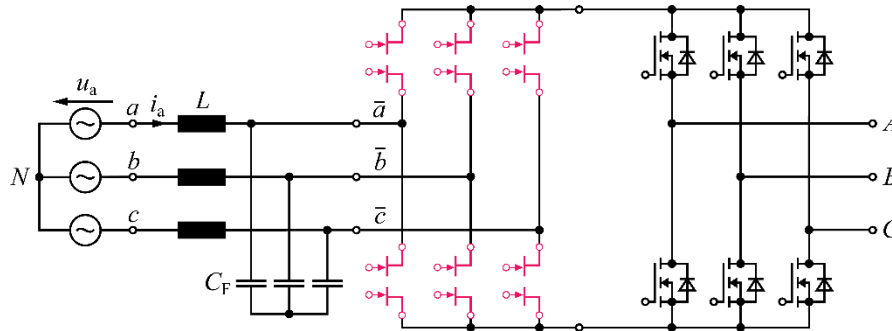


- **Input-Side Cap. / Output-Side Motor Ind. \rightarrow Operation Limited to Buck-Type (Step-Down) Conversion**

3- Φ AC/AC Matrix Converter Comparison

■ Indirect Matrix Converter (IMC)

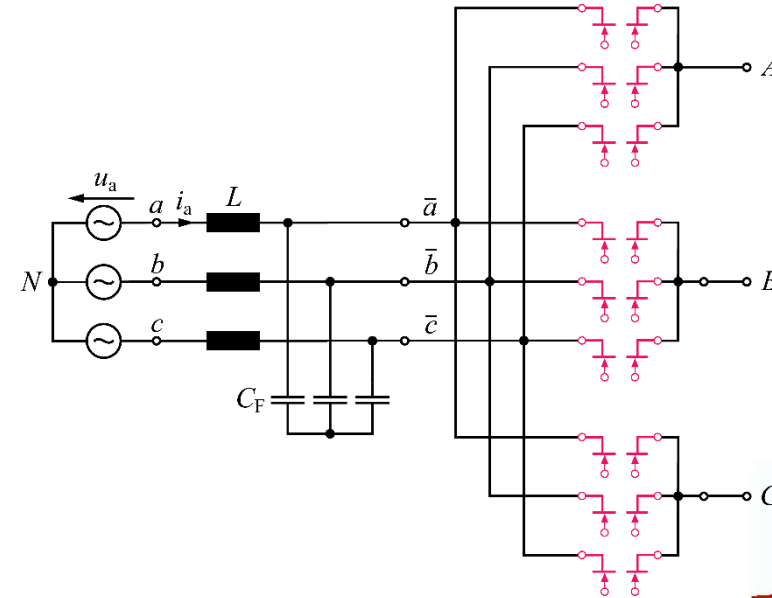
- GaN M-BDS AC/DC Front-End
- ZCS Commutation of AC/DC Stage @ $i_{DC}=0$
- No 4-Step Commutation



- Higher # of Switches Compared to DMC
- Lower Cond. Losses @ Low Output Voltage
- Thermally Critical @ $f_{out} \rightarrow 0$

■ Direct Matrix Converter (CMC)

- 4-Step Commutation
- Exclusive Use of GaN M-BDSs



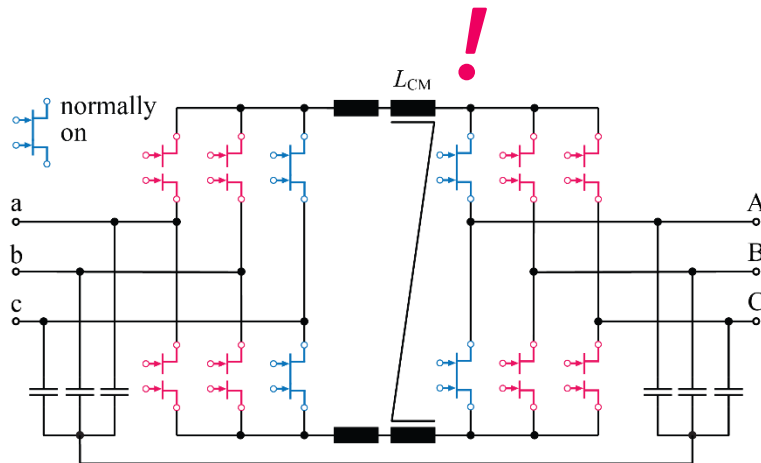
- Thermally Critical @ $f_{out} \approx f_{in}$



3- Φ Current DC-Link vs. Matrix AC/AC Converter

■ Current DC-Link Topology

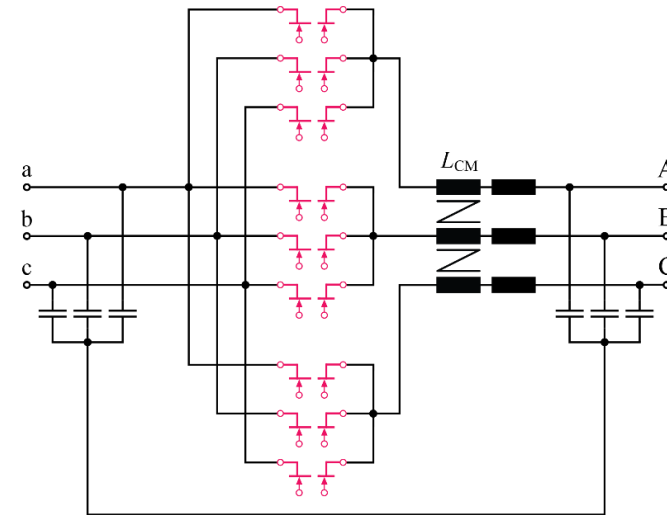
- Application of *M-BDSs* | 12 Switches
- 4-Step Commutation
- Buck-Boost Functionality
- Low Filter Volume



- Challenging *Overvoltage Protection*

■ Direct Matrix Converter

- Application of *M-BDSs* | 9 Switches
- 4-Step Commutation
- Complex Space Vector Modulation
- Limited to *Buck-Operation* (!)



- Challenging *Overvoltage Protection*



Outlook

Summary

■ *Future Need for „SWISS Knife“-Type Inverter Systems*

- *Wide Input / Output Voltage Range*
- *Continuous / Sinusoidal Output Voltage*
- *Electromagnetically „Quiet“ - No Shielded Cables*
- *“Plug & Play” / Non-Expert Installation*
- *SMART Motors / Cognitive VSDs*
- *On-Line Monitoring / Industry 4.0*

■ *Enabling Technologies*

- *SiC / GaN*
- *Advanced (Multi-Level) Topologies*
- *“Synergetic” Control*
- *Monolithic Bidirectional GaN*
- *Integration of Switches / Gate Drives / Sensing / Monitoring*
- *Adv. Modeling / Simulation / Optimization*
- *Machine Learning / AI*

■ *System Level → Distributed DC Bus Systems, Integration of Storage, etc.*

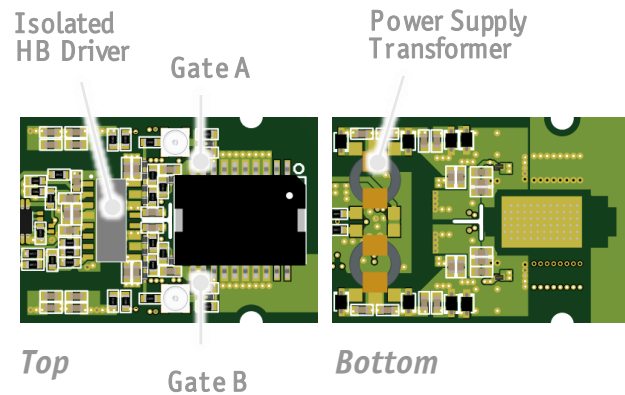


Source:
UK Outdoor
Store

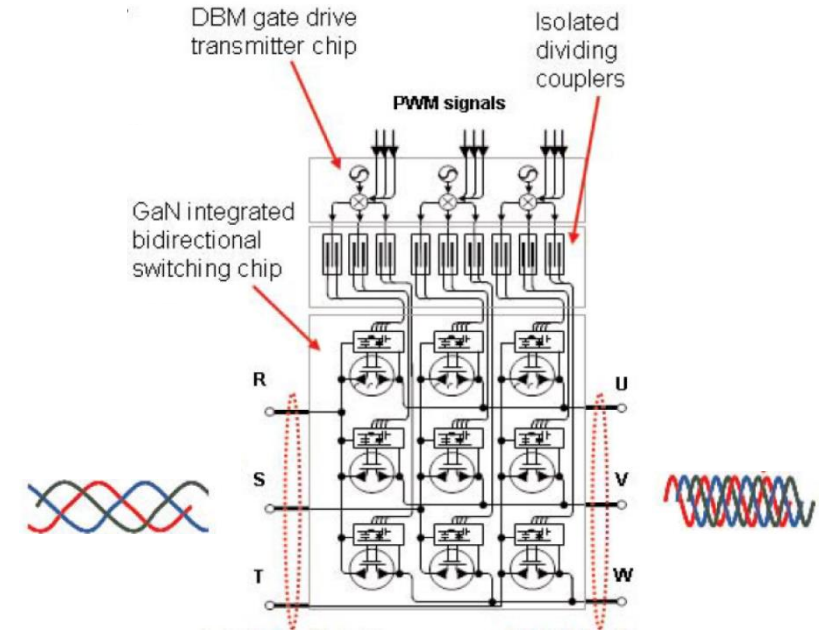
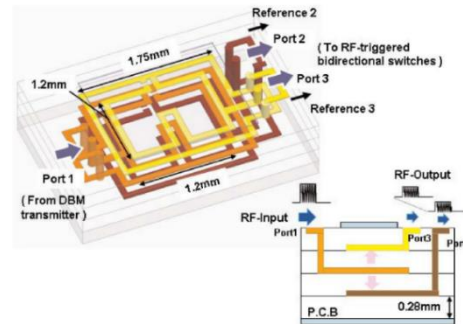
Monolithic 3D-Integration

Source: **Panasonic** ISSCC 2014

- **M-BDS GaN 3x3 Matrix Converter with Drive-By-Microwave (DBM) Technology**
- **9 Dual-Gate GaN AC-Switches / 4-Step Commutation**
- **DBM Gate Drive Transmitter Chip & Isolating Couplers**
- **Ultra Compact → 25 x 18 mm² (600V, 10A – 5kW Motor)**

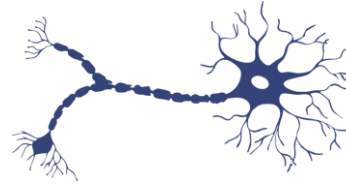


5.0GHz Isolated (5 kV_{DC}) Dividing Coupler



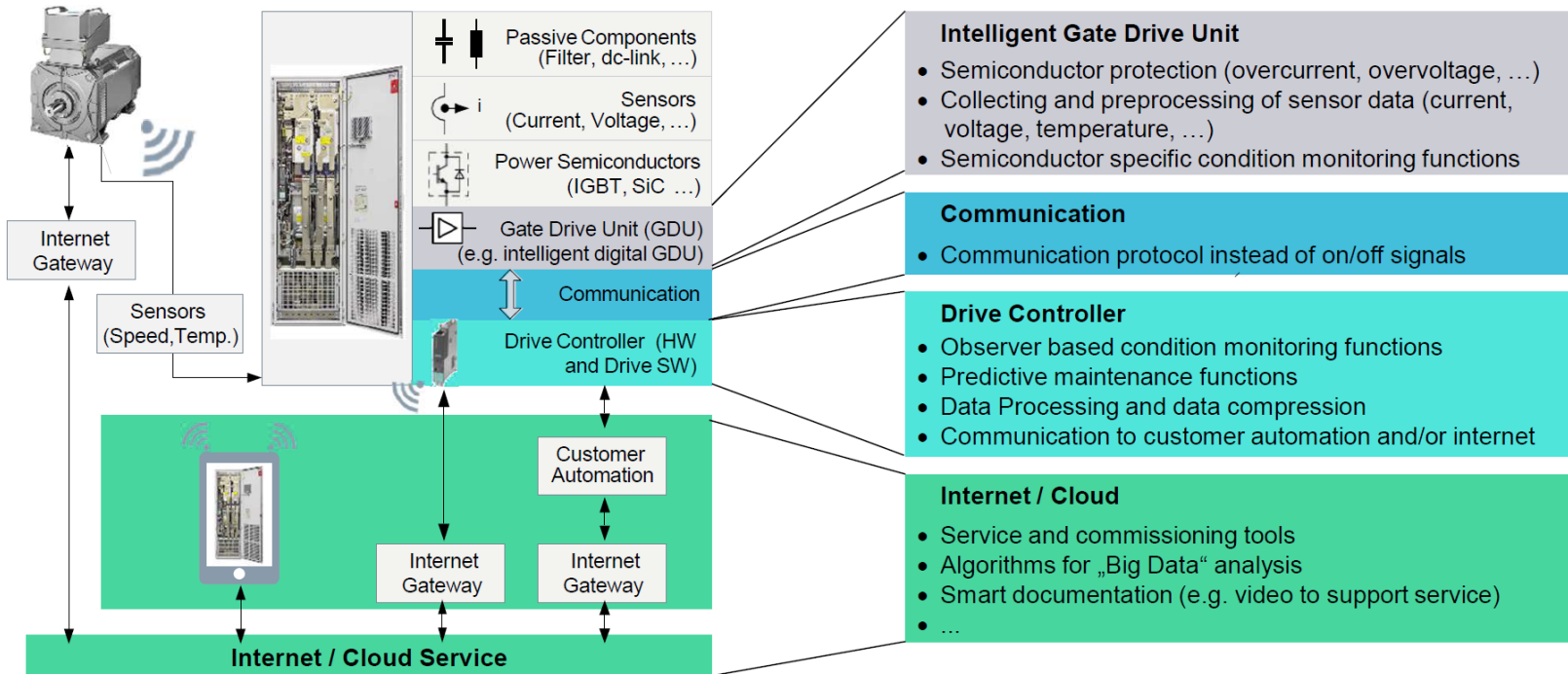
- **Massive Space Saving Compared to Discrete Realization (!)**

Smart Converter Concept



- Utilize High Computing Power & Network Effects in the Cloud → **“Cognitive” Power Electronics**

Source: Dr. R. Sommer
SIEMENS



- Sensing & Computing on **Component Level | Converter Level | System Level | Application Level**

Thank you!



Acknowledgement

M. Antivachis
J. Azurza
D. Bortis
M. Guacci
M. Haider
M. Kasper
J. Kaufmann
F. Krismer
D. Menzi
N. Nain
P. Niklaus
G. Rohner
D. Zhang

